1. Options for Calculations

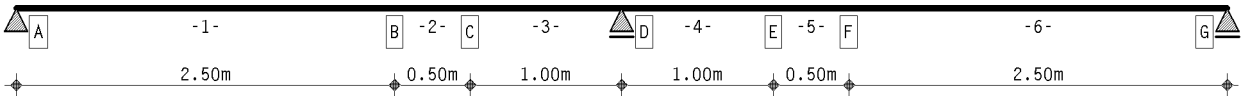
calculation acc. to DIN 1052:2008

service class 1

coefficients of thermal expansion: timber α_t = 0.500 *10^{-5}/°K, steel α_t = 1.200 *10^{-5}/°K

2. Structural system

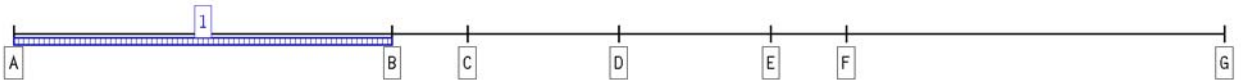
reinforcement left side



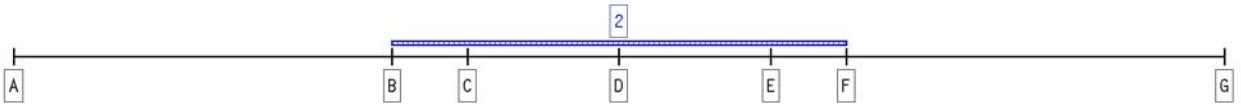
main beam

reinforcement right side

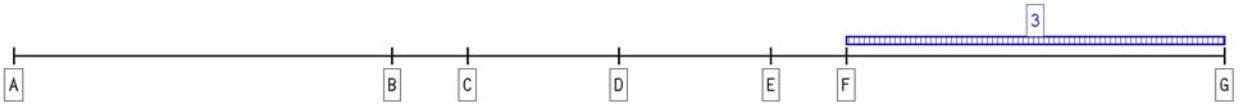
3. Loading



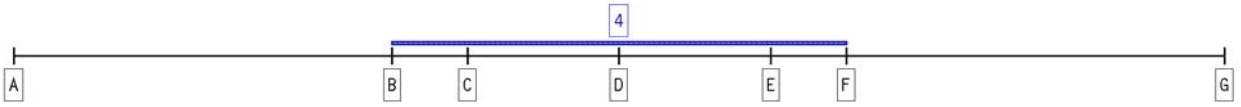
action effect 1: dead load (permanent, 5 load cases)



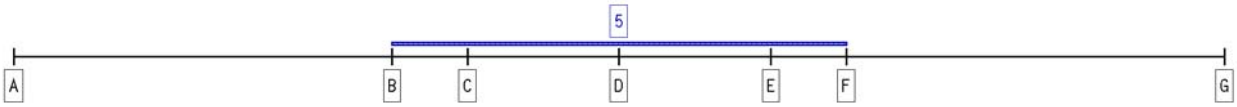
G



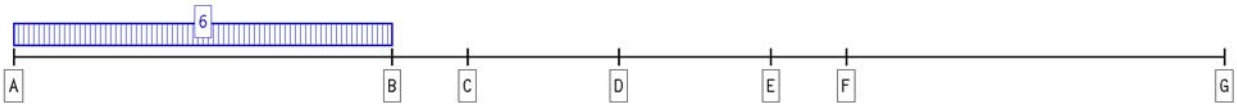
G



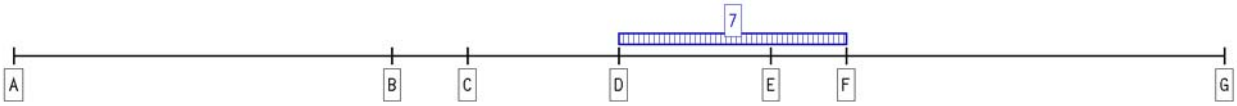
G



G



action effect 2: traffic (transient, 8 load cases)



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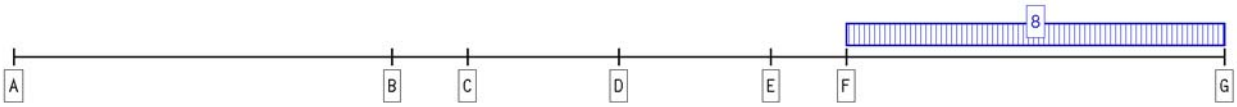

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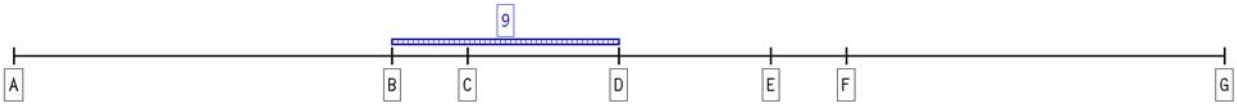
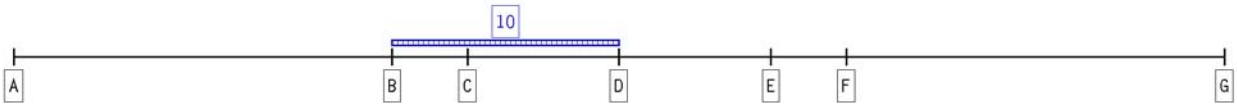
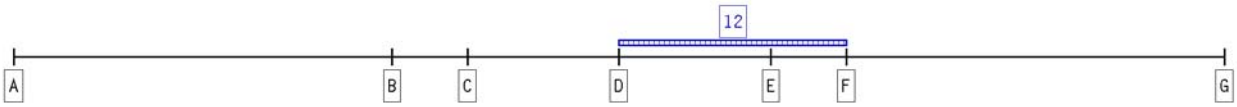


G



G



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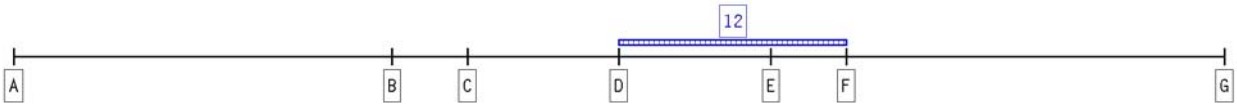
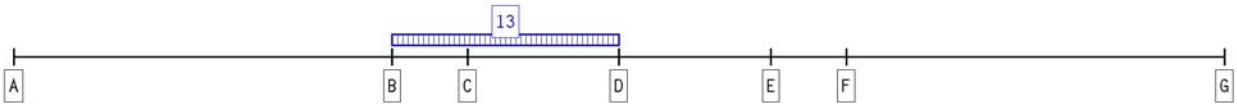
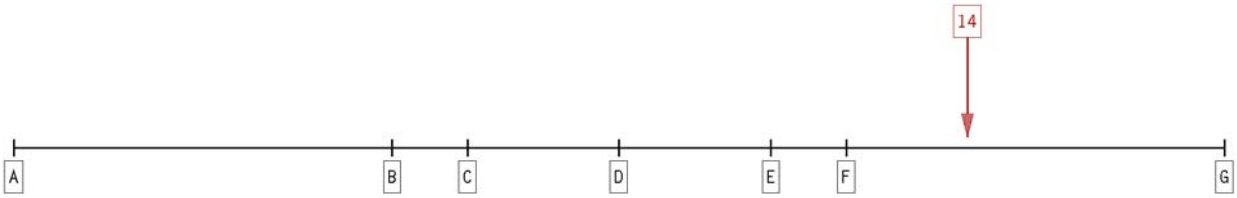


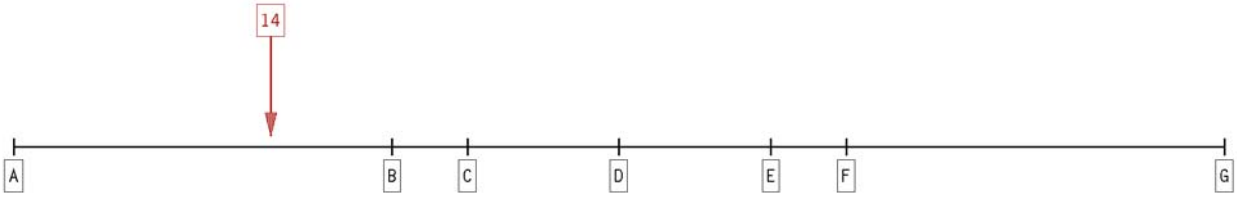
G



G



action effect 3: snow (transient, 1 load cases)

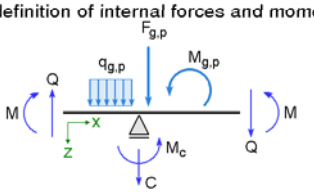


G

4. material parameters

timber grade main beam	solid coniferous timber, C24 (S10)
service class	1
beam width	b = 100 mm
coeff. therm.expan. timber:	0.500 *10-5 /°K
coeff. thermal expan. steel:	1.200 *10-5 /°K
char. bend. strength $f_{m,k}$:	24.0 N/mm²
char. shear strength $f_{v,k}$:	2.0 N/mm²
modulus of elast. $E_{0,mean}$:	11000 N/mm²

definition of internal forces and moments:



5. Beam sections

section beam section 2, scale 1: 5

section beam section 3, scale 1: 5

section beam section 4, scale 1: 5

section beam section 5, scale 1: 5

main beam sections

section	x_A m	x_E m	l m	l_{ef} m	k_m -	l_v m	cantil.	$h_{main\ beam}$ mm
1	0.00	2.50	2.50	4.00	1.0000	4.00	-	240
2	2.50	3.00	0.50	4.00	1.0000	4.00	-	240
3	3.00	4.00	1.00	4.00	1.0000	4.00	-	240
4	4.00	5.00	1.00	4.00	1.0000	4.00	-	240
5	5.00	5.50	0.50	4.00	1.0000	4.00	-	240
6	5.50	8.00	2.50	4.00	1.0000	4.00	-	240

sections with reinforcements

section	reinforcement left side	reinforcement right side
1	-	-
2	steel plate S235 (St37) 6/160 mm	steel plate S235 (St37) 6/160 mm
3	steel plate S235 (St37) 6/160 mm	steel plate S235 (St37) 6/160 mm
4	steel plate S235 (St37) 6/160 mm	steel plate S235 (St37) 6/160 mm
5	steel plate S235 (St37) 6/160 mm	steel plate S235 (St37) 6/160 mm
6	-	-

6. Fastener data

section 2 from x_A = 2.50 m to x_E = 3.00

bolt 20 mm, FK 5.8

1 - row, simplified verification acc. to DIN 1052:2008, 12.5.4(2)

f_{uk} = 500 N/mm², M_{yk} = 362051 Nmm

reduction of R_k with f = 0.843 for $vorht < t_{req}$

K_{ser} = 13096 N/mm, γ_M = 1.10, **R_k = 11970.0 N, all values per shear plane**

coordinates of connectors section 2

Nr.	x_{Abs} m	x_D m
1	0.100	2.600

section 3 from x_A = 3.00 m to x_E = 4.00

bolt 20 mm, FK 5.8

1 - row, simplified verification acc. to DIN 1052:2008, 12.5.4(2)

f_{uk} = 500 N/mm², M_{yk} = 362051 Nmm

reduction of R_k with f = 0.843 for $vorht < t_{req}$

K_{ser} = 13096 N/mm, γ_M = 1.10, **R_k = 11970.0 N, all values per shear plane**

coordinates of connectors section 3

Nr.	x_{Abs} m	x_D m
1	0.150	3.150
2	0.700	3.700

section 4 from x_A = 4.00 m to x_E = 5.00

bolt 20 mm, FK 5.8

1 - row, simplified verification acc. to DIN 1052:2008, 12.5.4(2)

f_{uk} = 500 N/mm², M_{yk} = 362051 Nmm

reduction of R_k with f = 0.843 for $vorht < t_{req}$

K_{ser} = 13096 N/mm, γ_M = 1.10, **R_k = 11970.0 N, all values per shear plane**

coordinates of connectors section 4

Nr.	x_{Abs} m	x_D m
1	0.300	4.300
2	0.850	4.850

section 5 from x_A = 5.00 m to x_E = 5.50
bolt 20 mm, FK 5.8
1 - row, simplified verification acc. to DIN 1052:2008, 12.5.4(2)
f_{uk} = 500 N/mm², M_{yk} = 362051 Nmm
reduction of R_k with f = 0.843 for t_{vorh} < t_{req}
K_{ser} = 13096 N/mm, γ_M = 1.10, **R_k = 11970.0 N, all values per shear plane**

coordinates of connectors section 5

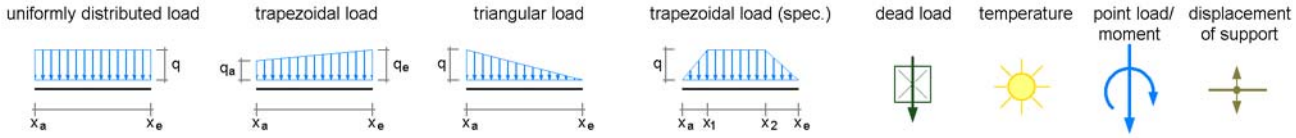
Nr.	x_{Abs} m	x_D m
1	0.400	5.400

7. Supports

coordinates of supports

supp.name	x m	c_F kN/m	c_M kNm/-	left reinf. (F)	left reinf. (M)	main beam (F)	main beam (M)	right reinf. (F)	right reinf. (M)
A	0.00	fix	----	-	-	X	-	-	-
D	4.00	fix	----	X	-	X	-	X	-
G	8.00	fix	----	-	-	X	-	-	-

8. Action effects



Permanent action effect: dead load
1. additive load case: permanent main beam 1
⇒ unif.distr.load (main beam): q = 1.60 kN/m from x_a = 0.00 m to x_e = 2.50 m
2. additive load case: permanent main beam 2
⇒ unif.distr.load (main beam): q = 0.80 kN/m from x_a = 2.50 m to x_e = 5.50 m
3. additive load case: permanent main beam 3
⇒ unif.distr.load (main beam): q = 1.60 kN/m from x_a = 5.50 m to x_e = 8.00 m
4. additive load case: permanent U140 left side
⇒ unif.distr.load (reinforcement left side): q = 0.50 kN/m from x_a = 2.50 m to x_e = 5.50 m
5. additive load case: permanent U140 right side
⇒ unif.distr.load (reinforcement right side): q = 0.50 kN/m from x_a = 2.50 m to x_e = 5.50 m

2. Transient action effect: traffic
6. additive load case: traffic main beam 1
⇒ unif.distr.load (main beam): q = 3.50 kN/m from x_a = 0.00 m to x_e = 2.50 m
7. additive load case: traffic main beam 2 a
⇒ unif.distr.load (main beam): q = 1.75 kN/m from x_a = 4.00 m to x_e = 5.50 m
8. additive load case: traffic main beam 3
⇒ unif.distr.load (main beam): q = 3.50 kN/m from x_a = 5.50 m to x_e = 8.00 m
9. additive load case: traffic U140 left side
⇒ unif.distr.load (reinforcement left side): q = 0.88 kN/m from x_a = 2.50 m to x_e = 4.00 m
10. additive load case: traffic U140 right side
⇒ unif.distr.load (reinforcement right side): q = 0.88 kN/m from x_a = 2.50 m to x_e = 4.00 m
12. additive load case: traffic U140 right side 2
⇒ unif.distr.load (reinforcement right side): q = 0.88 kN/m from x_a = 4.00 m to x_e = 5.50 m
⇒ unif.distr.load (reinforcement left side): q = 0.88 kN/m from x_a = 4.00 m to x_e = 5.50 m
13. additive load case: traffic main beam 2 b
⇒ unif.distr.load (main beam): q = 1.75 kN/m from x_a = 2.50 m to x_e = 4.00 m

3. Transient action effect: snow
14. additive load case: snow
⇒ point load (main beam): F = 8.00 kN at x = 6.30 m
⇒ point load (main beam): F = 8.00 kN at x = 1.70 m

9. verifications

1: DIN 1052:2008 load-carrying capacity
safety against overturning will be executed
buckling analysis of compression flange acc. to DIN 1052, 10.3.1 will be executed
verification of bearing stress DIN 1052, 10.2.4 will be executed
Extreme rule 1

2: DIN 1052:2008 deformations (rarely)
Extreme rule 1

3: DIN 1052:2008 deformations (quasicontinuous)
Extreme rule 1

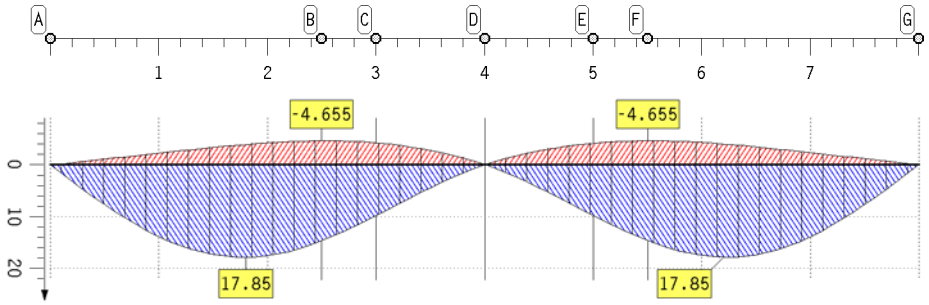
4: DIN 4102-22:2004-11 fire protection

fire resistance duration t_f = 30 min
combustion depth d_f = 2.40 cm
Abbrand 4-seitig
Extreme rule 1

10. Results of verification of ultimate limit state

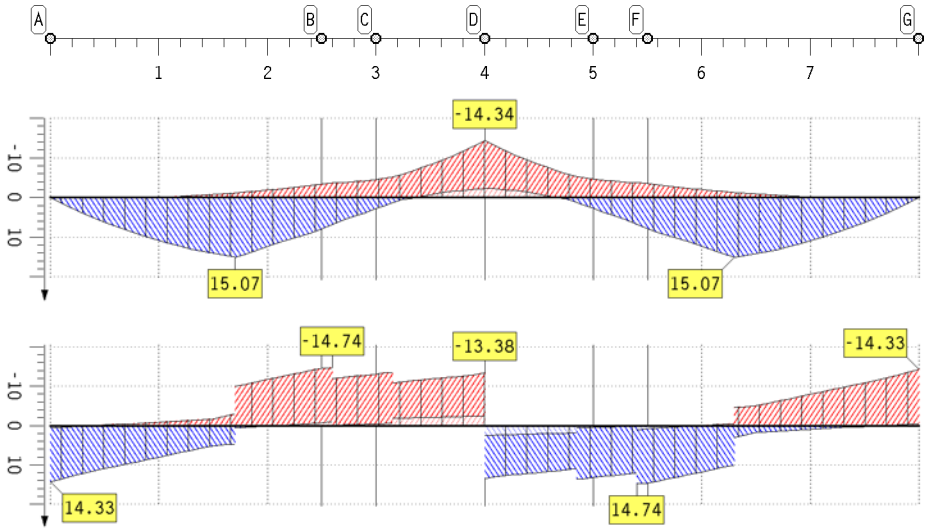
10.1. Verification of ultimate limit state

extremal deflections of main beam (incl. γ_F)



deflection
main beam
γ_F-fach
w in mm
Min: -4.66
Max: 17.85

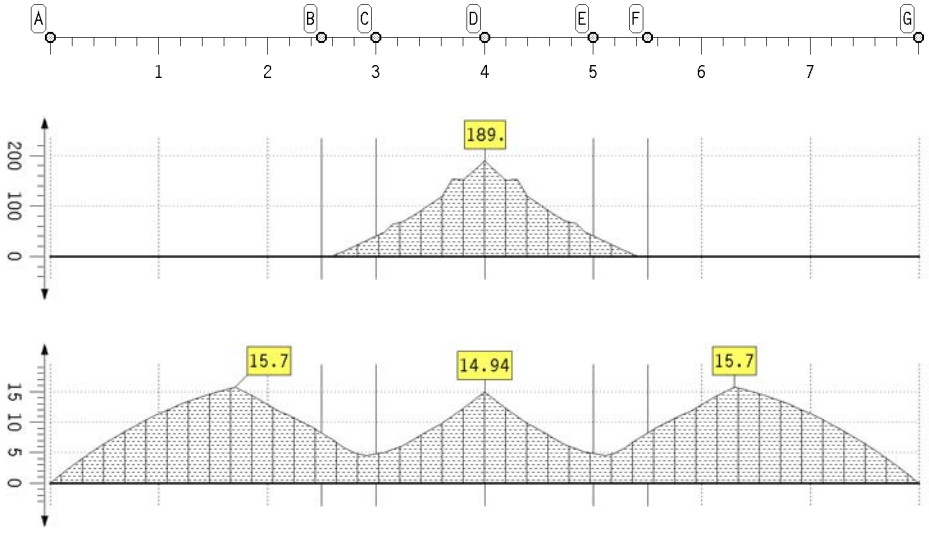
extremal internal forces



flexural moment
main beam
M in kNm
Min: -14.34
Max: 15.07

shear force
main beam
V in kN
Min: -14.74
Max: 14.74

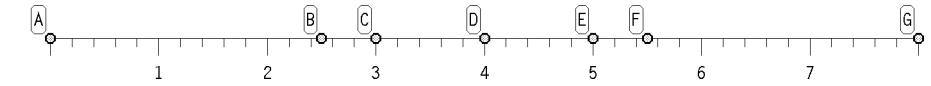
results of verification of ultimate limit state

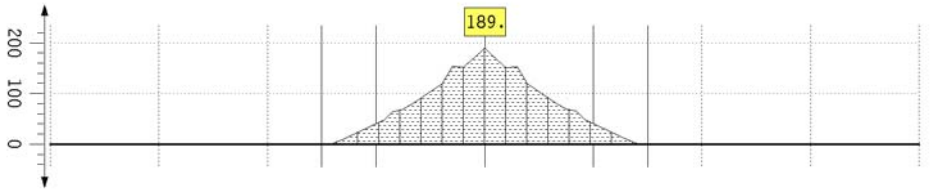


bending stress
reinf. left
σ_l in MN/m²
Max: 189.02

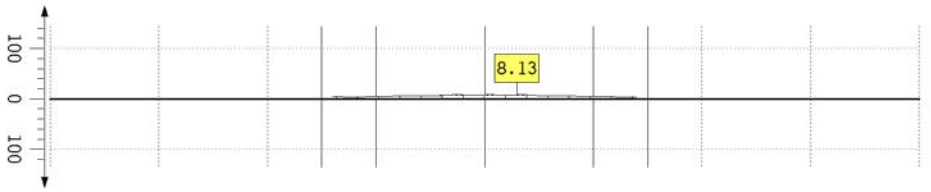
bending stress
main beam
σ_h in MN/m²
Max: 15.70

results of verification of ultimate limit state

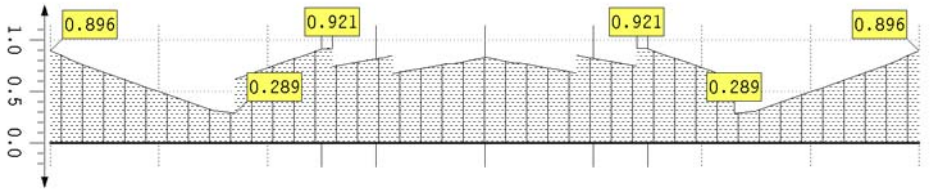




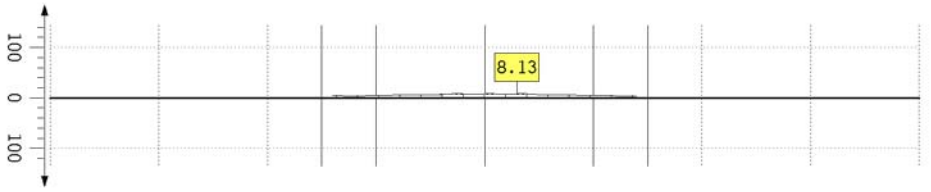
bending stress
reinf. right
σ_r in MN/m^2
Max: 189.02



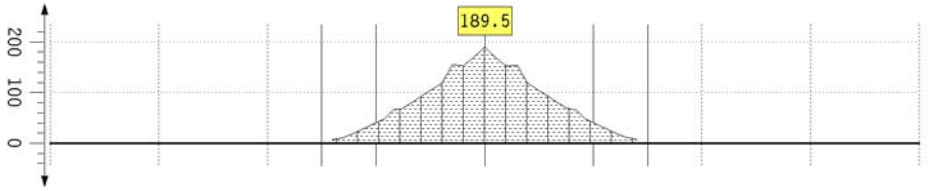
shear stress
reinf. left
τ_l in MN/m^2
Max: 8.13



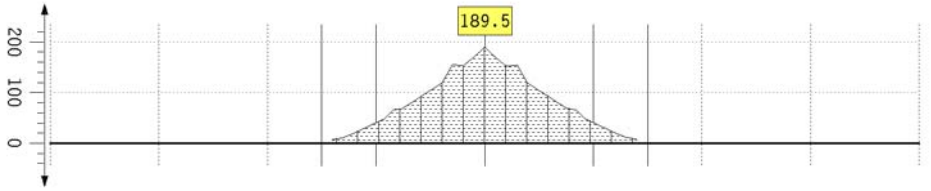
shear stress
main beam
τ_h in MN/m^2
Max: 0.92



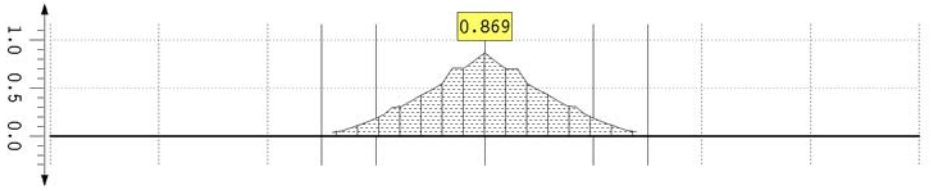
shear stress
reinf. right
τ_r in MN/m^2
Max: 8.13



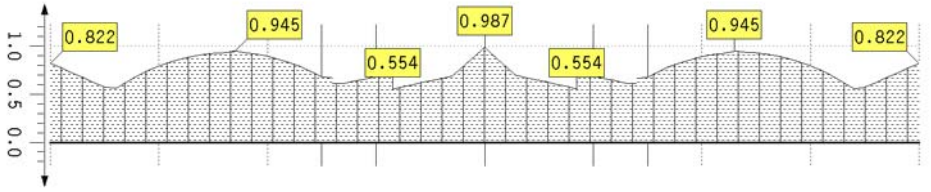
equivalent stress
reinf. left
$\sigma_{v,l}$ in MN/m^2
Max: 189.52



equivalent stress
$\sigma_{v,r}$ in MN/m^2
Max: 189.52

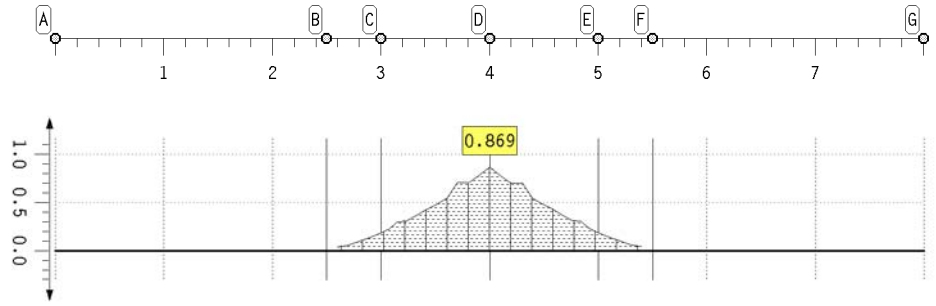


utilization
reinf. left
Max: 0.87



utilization
main beam
Max: 0.99

results of verification of ultimate limit state



utilization
reinf. right
Max: 0.87

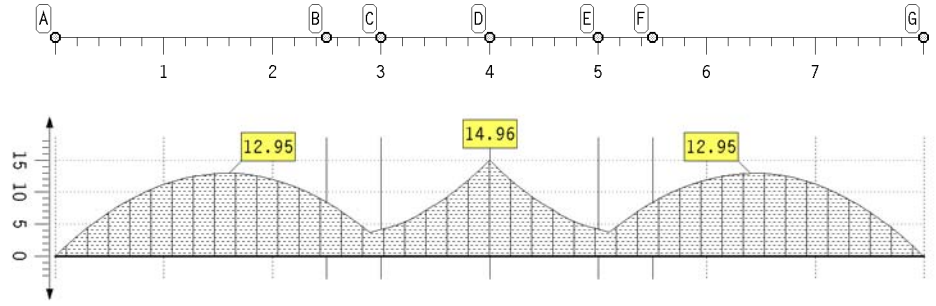
verification of bearing stress

support	l_{ef}	A_{ef}	A_P	k_{c90}	k_{mod}	f_{c90d}	σ_{c90d}	u
	mm	mm^2	N		-	N/mm^2	N/mm^2	-
A	---	---	---	---	---	---	---	---
D	---	---	---	---	---	---	---	---
G	---	---	---	---	---	---	---	---

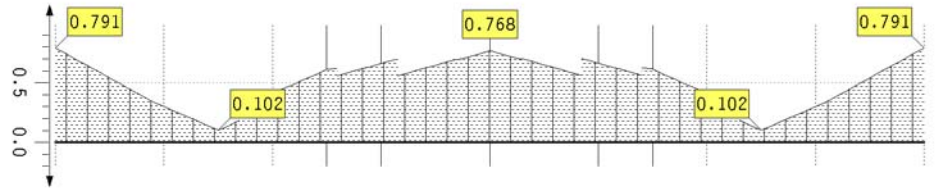
no verification of support(s) A, D, G!

11. Results of verification of fire protection

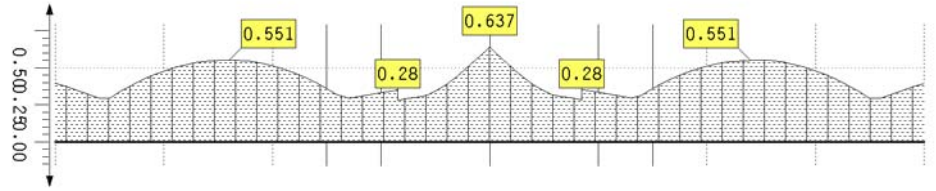
11.1. Verification of fire protection



bending stress
main beam
σ_h in MN/m^2
Max: 14.96



shear stress
main beam
τ_h in MN/m^2
Max: 0.79

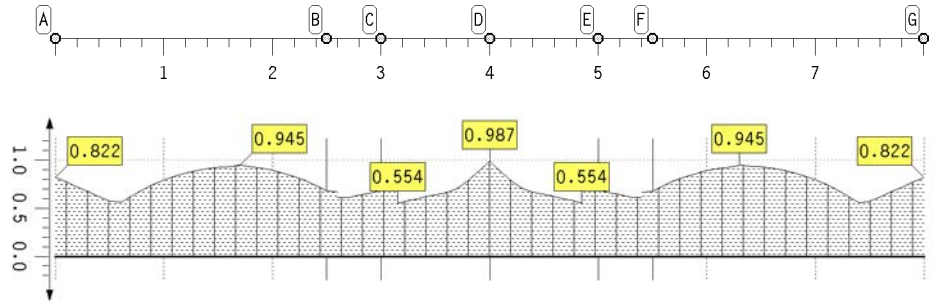


utilization
main beam
Max: 0.64

12. Summary

12.1. Summary of all verifications

maximal utilization



utilization
Max: 0.99

verification of bearing stress

support	l_{ef}	A_{ef}	A_P	k_{c90}	k_{mod}	f_{c90d}	σ_{c90d}	u
	mm	mm^2	N		-	N/mm^2	N/mm^2	-
A	---	---	---	---	---	---	---	---
D	---	---	---	---	---	---	---	---
G	---	---	---	---	---	---	---	---

no verification of support(s) A, D, G!

13. Utilizations of all verifications

all verifications successful!