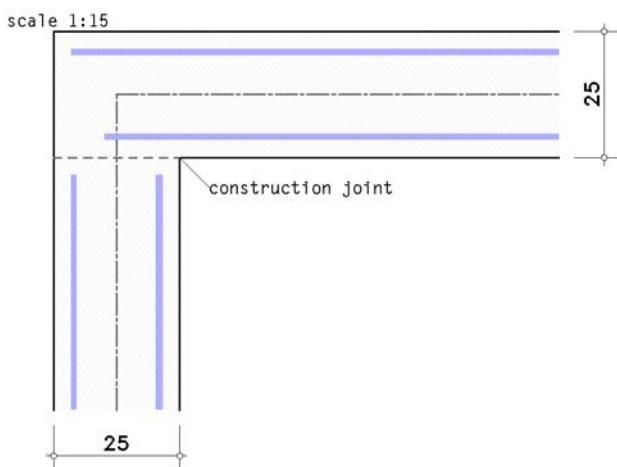


POS. 32: WOMMELSDORFF T.2, 16.3.1 (POS) WWW

dimensioning a frame corner EC 2 (1.11), NA: Deutschland

1. input protocol



system

beam: height $h_b = 25.0$ cm, axis distances (design calculation) $d_{1,bo} = 4.5$ cm, $d_{1,bu} = 4.5$ cm
column: height $h_c = 25.0$ cm, axis distances (design calculation) $d_{1,cl} = 4.5$ cm, $d_{1,cr} = 4.5$ cm
opening angle $\alpha = 90.00^\circ$, width beam/column $b_b = b_c = 100.0$ cm

material properties

concrete: C30/37, reinforcement: B500A

material safety factors

design situation: basic combination

design resistance: concrete $\gamma_c = 1.50$, reinforcement $\gamma_s = 1.15$

parameters

positive and negative moments are taken into account

req. reinforcement at the cut from bending and shear design (without minimum reinforcement):

shear design: compression strut angle simplified (EC 2-1-1 NA-DE, 6.2.3(2))

calculation of the required anchorage lengths: calculate bonding conditions

diameter of mandrel unabhängig vom concreterandabstand

beam-/column reinforcement from an external structural analysis

beam: above 5Ø12, bottom 10Ø12, stirrup Ø10/20.0 cm

column: left 7Ø10, right 8Ø12, stirrup Ø8/15.0 cm

design calculation values (ULS)

Ic 1: $N_{j,b,Ed} = 70.9$ kN, $M_{j,b,Ed} = 79.7$ kNm

1.1. durability and concrete cover

öffnendes Moment (Zug internal):

beam: minimum strength class, concrete cover

due to reinforcement corrosion XC2 \Rightarrow C16/20, $c_{nom} = 35$ mm, $c_{nom,l} = 22$ mm $\Rightarrow c_{nom} = 35$ mm $\leq c_v = 35$ mm **ok**

minimum concrete quality C16/20 with $f_{ck} = 16.0$ N/mm² < exst $f_{ck} = 30.0$ N/mm² **ok**

column: minimum strength class, concrete cover

due to reinforcement corrosion XC2 \Rightarrow C16/20, $c_{nom} = 35$ mm, $c_{nom,l} = 22$ mm $\Rightarrow c_{nom} = 35$ mm $\leq c_v = 35$ mm **ok**

minimum concrete quality C16/20 with $f_{ck} = 16.0$ N/mm² < exst $f_{ck} = 30.0$ N/mm² **ok**

2. note

general reinforcement rules are not taken into account.

3. design calculation

3.1. results table

design calculation values and required reinforcement

Ic	$N_{b,Ed}$ kN	$M_{b,Ed}$ kNm	$M_{c,Ed}$ kNm	$V_{c,Ed}$ kN	$A_{s,bu}$ cm ²	$A_{s,cr}$ cm ²	ΣA_s cm ²
1	70.9	79.7	70.8	70.9	9.99	8.02	18.02

$N_{b,Ed}$, $M_{b,Ed}$: design calculation values in the beam cut; $M_{c,Ed}$, $V_{c,Ed}$: design calculation values in the column cut

$A_{s,bu}$: req. reinforcement in beam; $A_{s,cr}$: req. reinforcement in column

ΣA_s : reinforcement sum

3.2. Ic 1 (decisive)

design calculation: $A_{s,bu} = 9.99 \text{ cm}^2$, $A_{s,cr} = 8.02 \text{ cm}^2$ ($\Sigma A_s = 18.02 \text{ cm}^2$)

4. final result

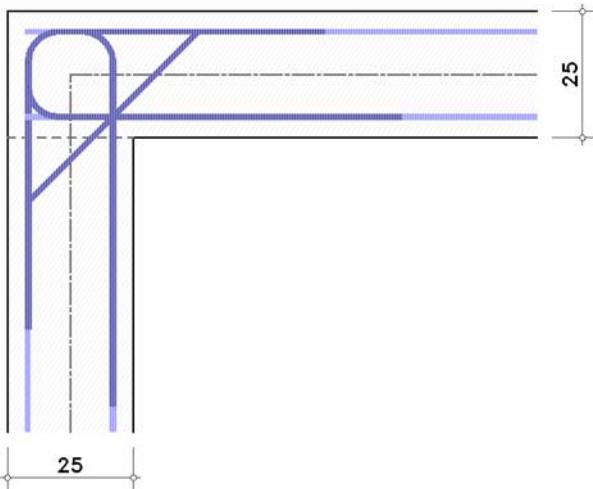
maximum reinforcement: $A_{s,bu} = 9.99 \text{ cm}^2$, $A_{s,cr} = 8.02 \text{ cm}^2$, $A_{s,s} = 5.00 \text{ cm}^2$

tensile splitting reinforcement horizontal fehlt !

tensile splitting reinforcement vertical fehlt !

5. selected reinforcement

scale 1:15



verification of reinforcement

concrete cover $c_v = 3.5 \text{ cm} = c_{nom} = 3.50 \text{ cm}$ ok

beam reinforcement:

above bar reinforcement, 5Ø12, exst $A_{s,bo} = 5.65 \text{ cm}^2$, req $A_{s,bo} = 0$
bar distance $s_{bo} = 22.9 \text{ cm} > \min s_{bo} = 3.2 \text{ cm}$ ok

bottom bar reinforcement, 10Ø12, exst $A_{s,bu} = 11.31 \text{ cm}^2 > \text{req } A_{s,bu} = 9.99 \text{ cm}^2$ ok
bar distance $s_{bu} = 10.2 \text{ cm} > \min s_{bu} = 3.2 \text{ cm}$ ok

column reinforcement:

left bar reinforcement, 7Ø10, exst $A_{s,cl} = 5.50 \text{ cm}^2$, req $A_{s,cl} = 0$
bar distance $s_{cl} = 15.3 \text{ cm} > \min s_{cl} = 3.0 \text{ cm}$ ok

right bar reinforcement, 8Ø12, exst $A_{s,cr} = 9.05 \text{ cm}^2 > \text{req } A_{s,cr} = 8.02 \text{ cm}^2$ ok
bar distance $s_{cr} = 13.1 \text{ cm} > \min s_{cr} = 3.2 \text{ cm}$ ok

tensile anchoring reinforcement of beam (bar reinforcement, 10Ø12, exst $A_{s,bu} = 11.31 \text{ cm}^2$, s. beam bottom):

lap length Zug $l_{b,bu,t} = 53.1 \text{ cm} = \text{req } l_{b,bu,t} = 53.1 \text{ cm}$ ok
compression $l_{b,bu,c} = 37.9 \text{ cm} = \text{req } l_{b,bu,c} = 37.9 \text{ cm}$ ok

diameter of mandrel $D_{bu} = 12.0 \text{ cm} = \text{req } D_{bu} = 12.0 \text{ cm}$ ok

U-bent length bottom $l_{bu} = h_c - c_v - \Phi b_{ü} + l_{b,bu,t} = 74.6 \text{ cm}$ (overlapping from the beam cut)
above $l_{bo} = h_c - c_v - \Phi b_{ü} + l_{b,bu,c} = 59.4 \text{ cm}$ (overlapping from the beam cut)

bar number $n_b = 10 < \text{perm } n_b = 21$ ok

tensile anchoring reinforcement of column (bar reinforcement, 8Ø12, exst $A_{s,cr} = 9.05 \text{ cm}^2$, s. column right):

lap length Zug $l_{b,cr,t} = 53.3 \text{ cm} = \text{req } l_{b,cr,t} = 53.3 \text{ cm}$ ok
compression $l_{b,cr,c} = 38.0 \text{ cm} = \text{req } l_{b,cr,c} = 38.0 \text{ cm}$ ok

diameter of mandrel $D_{cr} = 12.0 \text{ cm} = \text{req } D_{cr} = 12.0 \text{ cm}$ ok

U-bent length right $l_{cr} = h_b - c_v - \Phi b_{ü} + l_{b,cr} = 74.8 \text{ cm}$ (overlapping from the column cut)
left $l_{cl} = h_b - c_v - \Phi b_{ü} + l_{b,cl} = 59.5 \text{ cm}$ (overlapping from the column cut)

bar number $n_c = 8 < \text{perm } n_c = 21$ ok

transverse reinforcement:

bar reinforcement, 8Ø10, exst $A_{s,s} = 6.28 \text{ cm}^2 > \text{req } A_{s,s} = 5.00 \text{ cm}^2$ ok

bar distance $s_s = 13.1 \text{ cm} > \min s_s = 3.0 \text{ cm}$ ok

anchorage length beam $l_{b,s,b} = 28.8 \text{ cm} = \text{req } l_{b,s,b} = 28.8 \text{ cm}$ ok
column $l_{b,s,c} = 28.9 \text{ cm} = \text{req } l_{b,s,c} = 28.9 \text{ cm}$ ok

design resistance ensured

6. regulations

EN 1990, Eurocode 0: Grundlagen der Tragwerksplanung;

Deutsche Fassung EN 1990:2002 + A1:2005 + A1:2005/AC:2010, Ausgabe Dezember 2010

EN 1990/NA, Nationaler Anhang zur EN 1990, Ausgabe Dezember 2010

EN 1992-1-1, Eurocode 2: Bemessung und Konstruktion von Stahlbeton- und Spannbetonbauteilen - Teil 1-1: Allgemeine Bemessungsregeln und Regeln für den Hochbau;

