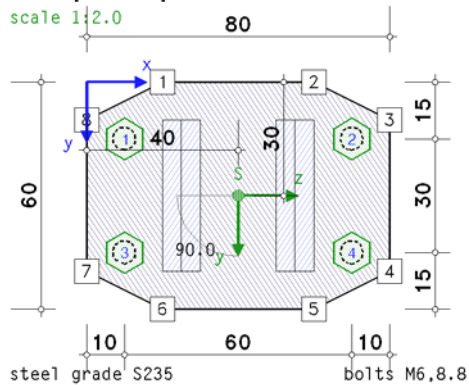


POS. 10: POLYPLATE DOUBLE SHEET

bolted end-plate connection EC 3-1-8 (12.10), NA: Deutschland

4H-EC3FS version: 2/2025-1b

1. input report



steel grade

steel grade S235

bolts

bolt class 8.8, bolt size M6, normal wrench size

shear plane passes through the unthreaded portion of the bolt

connection

end-plate (polygonal):

pt.	x _p mm	y _p mm	pt.	x _p mm	y _p mm
1	20.0	0.0	5	60.0	60.0
2	60.0	0.0	6	20.0	60.0
3	80.0	10.0	7	0.0	50.0
4	80.0	50.0	8	0.0	10.0

thickness $t_p = 8.0$ mm

beam: $h = 40.0$ mm, $b = 40.0$ mm, $A = 8.00$ cm², $y_s = -20.0$ mm, $z_s = 20.0$ mm

$I_y = 18.67$ cm⁴, $I_z = 10.67$ cm⁴, $I_T = 2.67$ cm⁴, $I_\omega = 24.00$ cm⁶

rotation of cross-section around section centroid $\beta = 90.0^\circ$

beam-end-plate: surrounding fillet weld, weld thickness $a = 4.0$ mm

beam section centric on end-plate (beam centroid in plate centre)

coordinates of the beam centroid on end-plate $x_s = 40.0$ mm, $y_s = 30.0$ mm

bolts:

uniform arrangement of bolts, 2 vertical and 2 horizontal rows

edge distances top $e_o = 15.0$ mm, below $e_u = 15.0$ mm

distances between bolts $p_{y,1-2} = 30.0$ mm

edge distances left $e_l = 10.0$ mm, right $e_r = 10.0$ mm

distances between bolts $p_{x,1-2} = 60.0$ mm

calculation

verification:

calculation of internal forces and moments (FEM) and verifications of resistance

verification of end-plate with the plastic method, verification of compression by contact

verification of beam section with the elastic method

verification of bolts, check of distances

FEM-calculation:

bolts are plastically calculated, spring constant of bolts $c_f = 1863.6$ kN/cm

plastic limit force $F_{t,f} = f_{t,f} \cdot F_{t,Rd} = 11.0$ kN, $f_{t,f} = 0.950$, $F_{t,Rd} = (k_2 \cdot f_{ub} \cdot A_s) / \gamma_{M2} = 11.58$ kN, $k_2 = 0.90$

effective elongation at failure $\epsilon_{t,f} = f_{t,e} \cdot \epsilon_{ub} = 3.0\%$, $f_{t,e} = 0.250$, $\epsilon_{ub} = 12.0\%$

without preloading ($F_{p,c} = 0$)

effective foundation modulus of end plate $c_b = 26250.0$ kN/cm³

number / dimension of finite elements each direction $n_x / \Delta x = 35 / 2.3$ mm, $n_y / \Delta y = 26 / 2.3$ mm

max. 50 iteration steps (tolerance limit 5%)

internal forces and moments referring to local axes of cross-section

Lk 1: $N_{Ed} = -0.35$ kN, $M_{y,Ed} = 0.38$ kNm, $V_{z,Ed} = 0.23$ kN

$M_{z,Ed} = 0.00$ kNm, $V_{y,Ed} = 0.00$ kN

Lk 2: $N_{Ed} = -0.88$ kN, $M_{y,Ed} = 0.29$ kNm, $V_{z,Ed} = 0.17$ kN

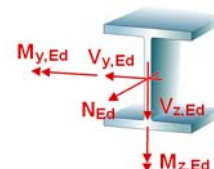
$M_{z,Ed} = 0.04$ kNm, $V_{y,Ed} = 0.02$ kN

Lk 3: $N_{Ed} = -0.88$ kN, $M_{y,Ed} = 0.07$ kNm, $V_{z,Ed} = 0.28$ kN

$M_{z,Ed} = -0.03$ kNm, $V_{y,Ed} = -0.02$ kN

partial safety factors for material

resistance of cross-sections $\gamma_{M0} = 1.00$



resistance of bolts, welds, plates in bearing $\gamma_{M2} = 1.25$

local stresses especially of the beam and of welds are not considered !

4H-QUER-cross-sections sind über ihre Mittellinien beschrieben.

edge- and distances between bolts sind daher separat zu überprüfen !!

FEM: the bolt distance from the free edge of the plate edge is too small (min $e = 8.9 \text{ mm} < 12.0 \text{ mm}$).
the accuracy of the results cannot be guaranteed !!

utilizations

in utilization of bolts due to tension $U_{t,s}$ ist minimum plastic utilization of the connection U_{pl} and plastic utilization of tensile forces of bolts $U_{pl,s}$ is included.

Lk	U_p	U_σ	U_b	$U_{pl,s}$	$U_{pl,t,s}$	$U_{wt,s}$	$U_{t,s}$	$U_{vt,s}$	$U_{b,s}$	U_q	U
1	0.331	0.331	0.100	0.220	0.361	0.044	0.088	0.250	0.003	0.176	0.361*
2	0.263	0.263	0.081	0.153	0.264	0.036	0.071	0.203	0.002	0.165	0.264
3	0.076	0.076	0.029	0.023	0.087	0.011	0.021	0.065	0.003	0.066	0.087

U_p : utilization of end-plate; U_σ : utilization of end-plate due to stress; U_b : utilization of end-plate due to compression by contact

$U_{pl,s}$: minimum plastic utilization of the connection; $U_{pl,t,s}$: plastic utilization of tensile forces of bolts; $U_{wt,s}$: utilization of bolts due to elongation

$U_{t,s}$: utilization of bolts due to tension; $U_{vt,s}$: utilization of bolts due to shear; $U_{b,s}$: utilization of bolts due to bearing resistance

U_q : stress utilization of the beam; U : total utilization

*) maximum utilization

2. final result

maximum utilization of end-plate due to 3 Lk: max U_p with corresponding values

node	x	y	u_z	b_z	m_{xx}	m_{yy}	m_{xy}	q_x	q_y	U_p
	mm	mm	mm	N/mm ²	kNm/m	kNm/m	kNm/m	kN/m	kN/m	
656	54.9	16.1	0.025	0.00	-1.40	-0.44	0.01	18.35	-1.70	0.331

x,y: node coordinates; u_z : deformations (lifting off positive); b_z : compression by contact (compression positive); m_{xx}, m_{yy}, m_{xy} : moments
 q_x, q_y : shear forces; q_x, q_y : shear forces; U_p : utilization of end-plate

maximum utilization of bolts due to 3 Lk: max U_s with corresponding values

	x	y	F_t	U_{wt}	U_{vt}	U_b	U_s
	mm	mm	kN				
1	10.0	15.0	0.01	---	0.006	0.003	0.088
2	70.0	15.0	3.97	0.044	0.250	0.002	0.250
3	10.0	45.0	0.01	---	0.006	0.003	0.088
4	70.0	45.0	3.97	0.044	0.250	0.002	0.250

x,y: bolt coordinates; F_t : bolt force; U_{wt} : utilization due to elongation; U_{vt} : utilization due to shear

U_b : utilization due to bearing resistance; U_s : utilization of bolts

maximum utilization of end-plate [Lk 1]

maximum utilization of bolts due to elongation [Lk 1]

maximum utilization of bolts [Lk 1]

maximum utilization of the beam [Lk 1]

maximum utilization [Lk 1]

max $U_p = 0.331 < 1$ ok

max $U_{wt,s} = 0.044 < 1$ ok

max $U_s = 0.361 < 1$ ok

max $(U_q, U_{ct}) = 0.176 < 1$ ok

max $U = 0.361 < 1$ ok

verification succeeded

3. Regulations

EN 1990, Eurocode 0: Grundlagen der Tragwerksplanung;

Deutsche Fassung EN 1990:2002 + A1:2005 + A1:2005/AC:2010, Ausgabe Dezember 2010

EN 1990/NA, Nationaler Anhang zur EN 1990, Ausgabe Dezember 2010

EN 1993-1-1, Eurocode 3: Bemessung und Konstruktion von Stahlbauten -

Teil 1-1: Allgemeine Bemessungsregeln und Regeln für den Hochbau;

Deutsche Fassung EN 1993-1-1:2005 + AC:2009, Ausgabe Dezember 2010

EN 1993-1-1/A1, Ergänzungen zur EN 1993-1-1, Ausgabe Juli 2014

EN 1993-1-1/NA, Nationaler Anhang zur EN 1993-1-1, Ausgabe Dezember 2018

EN 1993-1-8, Eurocode 3: Bemessung und Konstruktion von Stahlbauten -

Teil 1-8: Bemessung von Anschlüssen;

Deutsche Fassung EN 1993-1-8:2005 + AC:2009, Ausgabe Dezember 2010

EN 1993-1-8/NA, Nationaler Anhang zur EN 1993-1-8, Ausgabe Dezember 2010

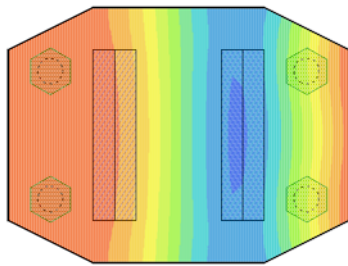
4. Lk 1 (decisive)

4.1. end-plate

design values: $N = -0.35 \text{ kN}$, $M_y = 0.38 \text{ kNm}$

deformations u_z [mm]

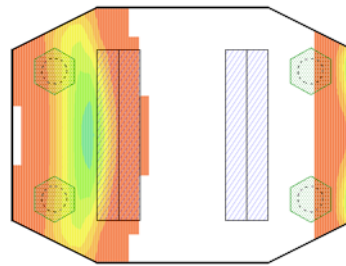
min $u_z = -0.0017 \text{ mm}$, max $u_z = 0.0256 \text{ mm}$



deformations lifting off positive

compression by contact b_z [N/mm²]

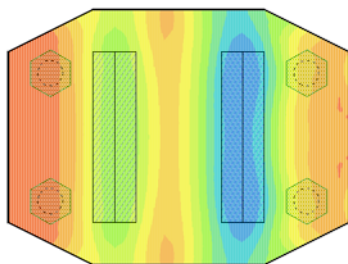
min $b_z = 0.00 \text{ N/mm}^2$, max $b_z = 23.58 \text{ N/mm}^2$



compression by contact compression positive

utilization of end-plate U_p

min $U_p = 0.000$, max $U_p = 0.331$



utilization of end-plate

node	x mm	y mm	u_z mm	b_z N/mm ²	U_p
602	50.3	16.1	0.025	0.00	0.292
656	54.9	16.1	0.025	0.00	0.331
952	80.0	13.8	-0.002	23.58	0.100

x,y: node coordinates; u_z : deformations (lifting off positive); b_z : compression by contact (compression positive); U_p : utilization of end-plate

utilization of bolts

	x mm	y mm	w_t mm	F_t kN	ε_{wt} %	U_{wt}
1	10.0	15.0	-0.000	0.01	0.000	---
2	70.0	15.0	0.011	3.97	0.133	0.044
3	10.0	45.0	-0.000	0.01	0.000	---
4	70.0	45.0	0.011	3.97	0.133	0.044

x,y: bolt coordinates; w_t : deformation (tension positive); F_t : bolt force; ε_{wt} : elongation
 U_{wt} : utilization due to elongation

utilization of end-plate [node 656] $U_{\max} = 0.331 < 1$ ok

utilization of bolts due to elongation [bolt 2] $U_{s,\max} = 0.044 < 1$ ok

minimum plastic utilization of bolts $U_{pl,s,\min} = 0.220 < 1$ ok

plastic utilization of tensile forces of bolts $U_{pl,t,s} = 0.361 < 1$ ok

4.2. bolts

design values: min $F_t = 0.01 \text{ kN}$, max $F_t = 3.97 \text{ kN}$, $V_z = 0.23 \text{ kN}$

verification of bolts

U_{tp} utilization due to punching shear failure, U_{vt} utilization due to shear in tension, U_b utilization due to bearing resistance, U utilization of bolts

bolt 1	$U_{tp,1} = 0.000$	$U_{vt,1} = 0.006$	$U_{b,1} = 0.003$	$U_1 = 0.006$
bolt 2	$U_{tp,2} = 0.088$	$U_{vt,2} = 0.250$	$U_{b,2} = 0.002$	$U_2 = 0.250$
bolt 3	$U_{tp,3} = 0.000$	$U_{vt,3} = 0.006$	$U_{b,3} = 0.003$	$U_3 = 0.006$
bolt 4	$U_{tp,4} = 0.088$	$U_{vt,4} = 0.250$	$U_{b,4} = 0.002$	$U_4 = 0.250$
total:	$U_{tp} = 0.088$	$U_{vt} = 0.250$	$U_b = 0.003$	$U = 0.250 < 1$ ok

in utilization of bolts max U_s the minimum plastic utilization of bolts min $U_{pl,s} = 0.220$

and plastic utilization of tensile forces of bolts $U_{pl,t,s} = 0.361$ is included.

utilization of bolts $U_{\max} = 0.361 < 1$ ok

4.3. beam

elastic verification for $N = -0.35 \text{ kN}$, $M_y = 0.38 \text{ kNm}$, $V_z = 0.23 \text{ kN}$

verification: $\sigma_v = 41.38 \text{ N/mm}^2 < \sigma_{v,Rd} = 235.00 \text{ N/mm}^2 \Rightarrow U_\sigma = 0.176 < 1$ ok

utilization of the beam $\max(U_\sigma, U_{c/t}) = 0.176 < 1$ ok

4.4. total

utilization Lk 1 $U_{\max} = 0.361 < 1$ ok