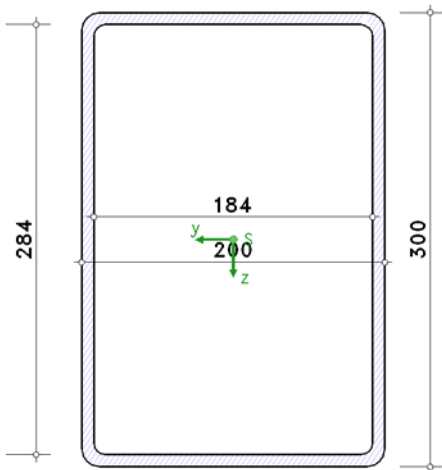


POS. 16: KINDMANN/KRÜGER 2.8.4

verification of cross-section EC 3-1-8 (12.10), NA: Deutschland

1. input report

scale 1:5.0



steel

steel grade S355

material safety factor

resistance of cross-sections $\gamma_{M0} = 1.00$

geometry

section RR 300 x 200 x 8.0(w)

resistance

elastic verification, calculation as thin-walled cross-section

valid normal, shear-, equivalent stress: $\sigma_{x,Rd} = 355.0 \text{ N/mm}^2$, $\tau_{Rd} = 205.0 \text{ N/mm}^2$, $\sigma_{v,Rd} = 355.0 \text{ N/mm}^2$

internal forces and moments referring to local axes of cross-section

σ -generating forces (N, M) work at centroid, τ -generating forces (V, T_t) work at shear center

Lk 1: $M_{y,Ed} = -20000.00 \text{ kNcm}$, $V_{z,Ed} = 40.00 \text{ kN}$, $T_{t,Ed} = 2000.00 \text{ kNcm}$

notes

buckling is not investigated.

2. Lk 1

2.1. verification of cross-section

internal forces and moments: $M_y = -20000.00 \text{ kNcm}$, $V_z = 40.00 \text{ kN}$, $T_t = 2000.00 \text{ kNcm}$

2.1.1. elastic verification

elastic verification for $M_y = -200.00 \text{ kNm}$, $V_z = 40.00 \text{ kN}$, $T_t = 20.00 \text{ kNm}$

elastic stresses: $\max |\sigma_x| = 308.74 \text{ N/mm}^2$, $\max \tau = 33.81 \text{ N/mm}^2$, $\max \sigma_v = 312.62 \text{ N/mm}^2$

$\max \sigma_x$ bei $y = -80.0 \text{ mm}$, $z = -150.0 \text{ mm}$: $\sigma_x = 308.74 \text{ N/mm}^2$, $\tau = 19.27 \text{ N/mm}^2$, $\sigma_v = 310.54 \text{ N/mm}^2$

$\min \sigma_x$ bei $y = 80.0 \text{ mm}$, $z = 150.0 \text{ mm}$: $\sigma_x = -308.74 \text{ N/mm}^2$, $\tau = 28.36 \text{ N/mm}^2$, $\sigma_v = 312.62 \text{ N/mm}^2$

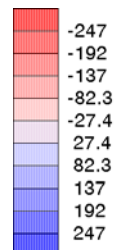
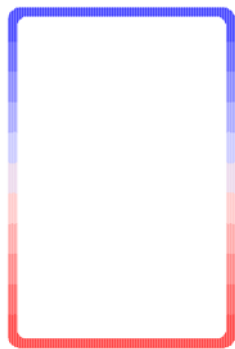
$\max \tau$ bei $y = 100.0 \text{ mm}$, $z = 0.0 \text{ mm}$: $\sigma_x = -0.00 \text{ N/mm}^2$, $\tau = 33.81 \text{ N/mm}^2$, $\sigma_v = 58.57 \text{ N/mm}^2$

$\max \sigma_v$ bei $y = 80.0 \text{ mm}$, $z = 150.0 \text{ mm}$: $\sigma_x = -308.74 \text{ N/mm}^2$, $\tau = 28.36 \text{ N/mm}^2$, $\sigma_v = 312.62 \text{ N/mm}^2$

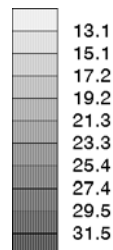
valid equivalent stress: $\sigma_{v,Rd} = 355.0 \text{ N/mm}^2$

verification: $\sigma_v = 312.62 \text{ N/mm}^2 < \sigma_{v,Rd} = 355.00 \text{ N/mm}^2 \Rightarrow U_\sigma = 0.881 < 1$ **ok**

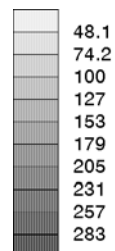
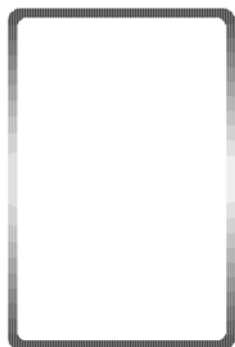
normal stresses σ_x [N/mm²]
min $\sigma_x = -308.8$, max $\sigma_x = 308.8$



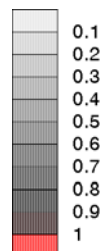
shear stresses τ [N/mm²]
max $\tau = 33.8$



equivalent stresses σ_v [N/mm²]
max $\sigma_v = 312.9$



utilization U_σ
max $U_\sigma = 0.881$



stresses, utilizations

y mm	z mm	σ_x N/mm ²	τ N/mm ²	σ_v N/mm ²	U_σ
-12.0	300.0	-308.80	29.03	312.87	0.881
-11.5	300.0	-308.80	29.04	312.87	0.881
-188.0	0.0	308.80	18.61	310.48	0.875
0.0	150.0	0.00	33.82	58.58	0.165

y,z: node coordinates; σ_x, τ, σ_v : stresses; U_σ : stress utilization

3. final result

maximum utilization: resistance max $U = 0.881 < 1$ ok

verification succeeded