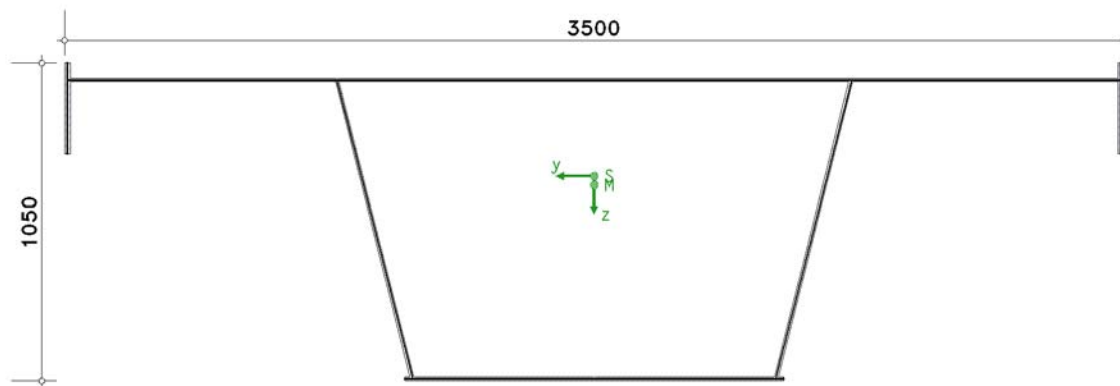


POS. 20: KINDMANN/KRÜGER 2.8.8

verification of cross-section EC 3-1-8 (12.10), NA: Deutschland

1. input report



steel

steel grade S235

material safety factor

resistance of cross-sections $\gamma_{M0} = 1.00$

geometry

dimensions of cross-section: $y_{min} = -1750.0$ mm, $y_{max} = 1750.0$ mm, $z_{min} = -56.0$ mm, $z_{max} = 994.0$ mm

width,height of cross-section: $b = 3500.0$ mm, $h = 1050.0$ mm

centroid, rotation angle of main axis: $e_y = 0.0$ mm, $e_z = 318.4$ mm, $\alpha = 0.00^\circ$



cross-sectional area	A	=	951.34 cm ²
bending moment of inertia	I_η	=	1536874.74 cm ⁴
bending moment of inertia	I_ζ	=	9283406.01 cm ⁴
section modulus	$W_{\eta+}$	=	22747.61 cm ³
section modulus	$W_{\eta-}$	=	41051.23 cm ³
section modulus	$W_{\zeta+}$	=	53048.03 cm ³
section modulus	$W_{\zeta-}$	=	53048.03 cm ³
torsional moment of inertia	I_T	=	2063865.66 cm ⁴

resistance

elastic verification, calculation as thin-walled cross-section

valid normal, shear-, equivalent stress: $\sigma_{x,Rd} = 235.0$ N/mm², $\tau_{Rd} = 135.7$ N/mm², $\sigma_{v,Rd} = 235.0$ N/mm²

internal forces and moments referring to local axes of cross-section

σ -generating forces (N, M) work at centroid, τ -generating forces (V, T_t) work at shear center

Lk 1: $N_{Ed} = 50.00$ kN, $M_{y,Ed} = 4200.00$ kNm, $V_{z,Ed} = 230.00$ kN, $M_{z,Ed} = 205.00$ kNm, $V_{y,Ed} = 60.00$ kN
 $T_{t,Ed} = 160.00$ kNm

Lk 2: N, M_y, M_z

$N_{Ed} = 50.00$ kN, $M_{y,Ed} = 4200.00$ kNm, $M_{z,Ed} = 205.00$ kNm

Lk 3: V_z, V_y

$V_{z,Ed} = 230.00$ kN, $V_{y,Ed} = 60.00$ kN

Lk 4: T_t

$T_{t,Ed} = 160.00$ kNm

notes

buckling is not investigated.

2. Lk 1

2.1. verification of cross-section

internal forces and moments: $N = 50.00$ kN, $M_y = 4200.00$ kNm, $V_z = 230.00$ kN, $M_z = 205.00$ kNm, $V_y = 60.00$ kN, $T_t = 160.00$ kNm

2.1.1. elastic verification

elastic verification for $N = 50.00 \text{ kN}$, $M_y = 4200.00 \text{ kNm}$, $V_z = 230.00 \text{ kN}$, $M_z = 205.00 \text{ kNm}$

$V_y = 60.00 \text{ kN}$, $T_t = 160.00 \text{ kNm}$

elastic stresses: $\max |\sigma_x| = 186.54 \text{ N/mm}^2$, $\max \tau = 14.97 \text{ N/mm}^2$, $\max \sigma_v = 186.54 \text{ N/mm}^2$

$\max \sigma_x$ bei $y = -625.0 \text{ mm}$, $z = 675.6 \text{ mm}$: $\sigma_x = 186.54 \text{ N/mm}^2$, $\tau = 0.11 \text{ N/mm}^2$, $\sigma_v = 186.54 \text{ N/mm}^2$

$\min \sigma_x$ bei $y = 1750.0 \text{ mm}$, $z = -374.4 \text{ mm}$: $\sigma_x = -105.65 \text{ N/mm}^2$, $\tau = -0.16 \text{ N/mm}^2$, $\sigma_v = 105.65 \text{ N/mm}^2$

$\max \tau$ bei $y = 780.7 \text{ mm}$, $z = -20.2 \text{ mm}$: $\sigma_x = -6.71 \text{ N/mm}^2$, $\tau = 14.97 \text{ N/mm}^2$, $\sigma_v = 26.79 \text{ N/mm}^2$

$\max \sigma_v$ bei $y = -625.0 \text{ mm}$, $z = 675.6 \text{ mm}$: $\sigma_x = 186.54 \text{ N/mm}^2$, $\tau = 0.11 \text{ N/mm}^2$, $\sigma_v = 186.54 \text{ N/mm}^2$

valid equivalent stress: $\sigma_{v,Rd} = 235.0 \text{ N/mm}^2$

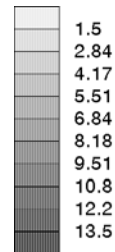
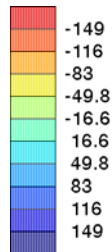
verification: $\sigma_v = 186.54 \text{ N/mm}^2 < \sigma_{v,Rd} = 235.00 \text{ N/mm}^2 \Rightarrow U_\sigma = 0.794 < 1$ **ok**

normal stresses σ_x [N/mm²]

$\min \sigma_x = -104.2$, $\max \sigma_x = 186.8$

shear stresses τ [N/mm²]

$\max \tau = 15.0$

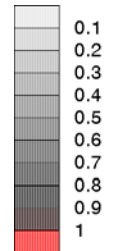
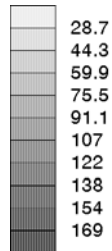


equivalent stresses σ_v [N/mm²]

$\max \sigma_v = 186.8$

utilization U_σ

$\max U_\sigma = 0.795$



stresses, utilizations

y mm	z mm	σ_x N/mm ²	τ N/mm ²	σ_v N/mm ²	U_σ	y mm	z mm	σ_x N/mm ²	τ N/mm ²	σ_v N/mm ²	U_σ
-20.0	0.0	-104.17	0.16	104.17	0.443	-2375.0	1043.0	186.76	0.00	186.76	0.795
-969.3	354.2	-5.31	15.02	26.55	0.113	-2355.0	1050.0	186.76	0.35	186.76	0.795
-2375.0	1050.0	186.76	0.16	186.76	0.795						

y,z: node coordinates; σ_x, τ, σ_v : stresses; U_σ : stress utilization

3. Lk 2: N,My,Mz

3.1. verification of cross-section

internal forces and moments: $N = 50.00 \text{ kN}$, $M_y = 4200.00 \text{ kNm}$, $M_z = 205.00 \text{ kNm}$

3.1.1. elastic verification

elastic verification for $N = 50.00 \text{ kN}$, $M_y = 4200.00 \text{ kNm}$, $M_z = 205.00 \text{ kNm}$

elastic stresses: $\max |\sigma_x| = 186.54 \text{ N/mm}^2$, $\max \tau = 0.00 \text{ N/mm}^2$, $\max \sigma_v = 186.54 \text{ N/mm}^2$

$\max \sigma_x$ bei $y = -625.0 \text{ mm}$, $z = 675.6 \text{ mm}$: $\sigma_x = 186.54 \text{ N/mm}^2$, $\tau = 0.00 \text{ N/mm}^2$, $\sigma_v = 186.54 \text{ N/mm}^2$

$\min \sigma_x$ bei $y = 1750.0 \text{ mm}$, $z = -374.4 \text{ mm}$: $\sigma_x = -105.65 \text{ N/mm}^2$, $\tau = 0.00 \text{ N/mm}^2$, $\sigma_v = 105.65 \text{ N/mm}^2$

$\max \sigma_v$ bei $y = -625.0 \text{ mm}$, $z = 675.6 \text{ mm}$: $\sigma_x = 186.54 \text{ N/mm}^2$, $\tau = 0.00 \text{ N/mm}^2$, $\sigma_v = 186.54 \text{ N/mm}^2$

valid equivalent stress: $\sigma_{v,Rd} = 235.0 \text{ N/mm}^2$

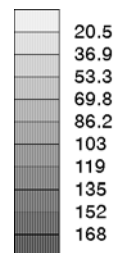
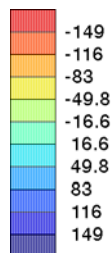
verification: $\sigma_v = 186.54 \text{ N/mm}^2 < \sigma_{v,Rd} = 235.00 \text{ N/mm}^2 \Rightarrow U_\sigma = 0.794 < 1$ **ok**

normal stresses σ_x [N/mm²]

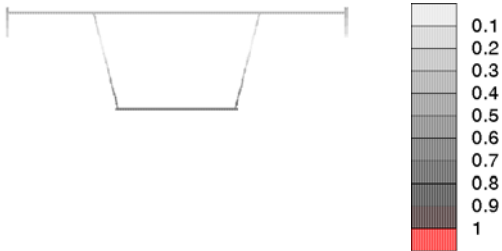
$\min \sigma_x = -104.2$, $\max \sigma_x = 186.8$

equivalent stresses σ_v [N/mm²]

$\max \sigma_v = 186.8$



utilization U_σ
max $U_\sigma = 0.795$



stresses, utilizations

y mm	z mm	σ_x N/mm ²	σ_y N/mm ²	U_σ
-20.0	0.0	-104.17	104.17	0.443
-2375.0	1050.0	186.76	186.76	0.795
-2375.0	1043.0	186.76	186.76	0.795
-2355.0	1050.0	186.76	186.76	0.795

y,z: node coordinates; σ_x, σ_y : stresses; U_σ : stress utilization

4. Lk 3: V_z, V_y

4.1. verification of cross-section

internal forces and moments: $V_z = 230.00$ kN, $V_y = 60.00$ kN

4.1.1. elastic verification

elastic verification for $V_z = 230.00$ kN, $V_y = 60.00$ kN

elastic stresses: max $|\sigma_x| = 0.00$ N/mm², max $\tau = 11.12$ N/mm², max $\sigma_v = 19.26$ N/mm²

max τ bei $y = -750.0$ mm, $z = 76.4$ mm: $\sigma_x = 0.00$ N/mm², $\tau = 11.12$ N/mm², $\sigma_v = 19.26$ N/mm²

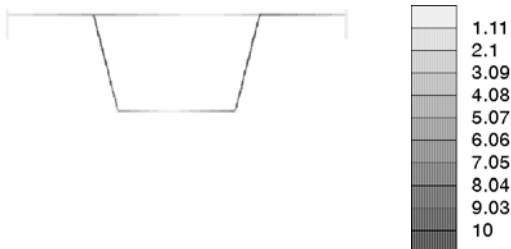
max σ_v bei $y = -750.0$ mm, $z = 76.4$ mm: $\sigma_x = 0.00$ N/mm², $\tau = 11.12$ N/mm², $\sigma_v = 19.26$ N/mm²

valid equivalent stress: $\sigma_{v,Rd} = 235.0$ N/mm²

verification: $\sigma_v = 19.26$ N/mm² < $\sigma_{v,Rd} = 235.00$ N/mm² $\Rightarrow U_\sigma = 0.082 < 1$ **ok**

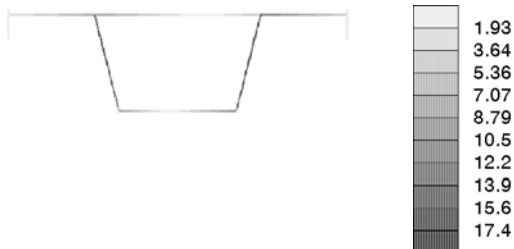
shear stresses τ [N/mm²]

max $\tau = 11.1$



equivalent stresses σ_v [N/mm²]

max $\sigma_v = 19.3$



utilization U_σ
max $U_\sigma = 0.082$



stresses, utilizations

y mm	z mm	τ N/mm ²	σ_v N/mm ²	U_σ
-2509.1	402.5	11.13	19.28	0.082
-2512.5	401.4	11.13	19.28	0.082
-2505.9	402.9	11.13	19.29	0.082

y,z: node coordinates; τ, σ_v : stresses; U_σ : stress utilization

5. Lk 4: Tt

5.1. verification of cross-section

internal forces and moments: $T_t = 160.00 \text{ kNm}$

5.1.1. elastic verification

elastic verification for $T_t = 160.00 \text{ kNm}$

elastic stresses: $\max |\sigma_x| = 0.00 \text{ N/mm}^2$, $\max \tau = 4.75 \text{ N/mm}^2$, $\max \sigma_v = 8.23 \text{ N/mm}^2$

$\max \sigma_v$ bei $y = 0.0 \text{ mm}$, $z = -324.4 \text{ mm}$: $\sigma_x = 0.00 \text{ N/mm}^2$, $\tau = 4.75 \text{ N/mm}^2$, $\sigma_v = 8.23 \text{ N/mm}^2$

valid equivalent stress: $\sigma_{v,Rd} = 235.0 \text{ N/mm}^2$

verification: $\sigma_v = 8.23 \text{ N/mm}^2 < \sigma_{v,Rd} = 235.00 \text{ N/mm}^2 \Rightarrow U_\sigma = 0.035 < 1$ **ok**

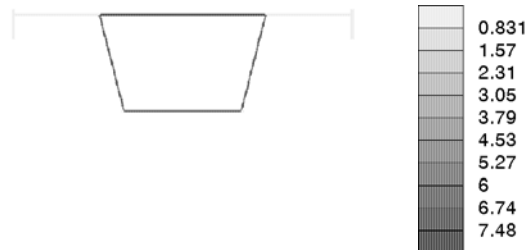
shear stresses τ [N/mm²]

$\max \tau = 4.8$



equivalent stresses σ_v [N/mm²]

$\max \sigma_v = 8.3$



utilization U_σ

$\max U_\sigma = 0.035$



stresses, utilizations

y mm	z mm	τ N/mm ²	σ_v N/mm ²	U_σ
-1750.0	50.0	4.80	8.31	0.035
-900.0	50.0	4.80	8.31	0.035
-1665.0	50.0	4.80	8.31	0.035

y,z: node coordinates; τ, σ_v : stresses; U_σ : stress utilization

6. final result

maximum utilization [Lk 1]: resistance $\max U = 0.794 < 1$ **ok**

verification succeeded