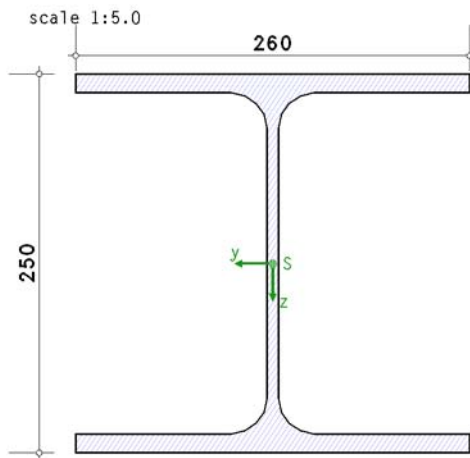


## POS. 7: WAGENKNECHT 8.4.2

verification of cross-section EC 3-1-8 (12.10), NA: Deutschland

### 1. input report



#### steel

steel grade S235

#### material safety factor

resistance of cross-sections  $\gamma_{M0} = 1.00$

#### geometry

section HE260A

#### resistance

elastic verification, calculation as thin-walled cross-section

valid normal, shear-, equivalent stress:  $\sigma_{x,Rd} = 235.0 \text{ N/mm}^2$ ,  $\tau_{Rd} = 135.7 \text{ N/mm}^2$ ,  $\sigma_{v,Rd} = 235.0 \text{ N/mm}^2$

#### internal forces and moments referring to main axes

$\sigma$ -generating forces (N, M) work at centroid,  $\tau$ -generating forces (V,  $T_t$ ) work at shear center

warping forces ( $T_\omega$ , B) work at shear center

Lk 1: Stelle 1

$T_{t,Ed} = 315.00 \text{ kNcm}$ ,  $T_{\omega,Ed} = 135.00 \text{ kNcm}$

Lk 2: Stelle 2

$T_{\omega,Ed} = 450.00 \text{ kNcm}$ ,  $B_{Ed} = 68700.00 \text{ kNcm}^2$

#### notes

buckling is not investigated.

### 2. Lk 1: Stelle 1

#### 2.1. verification of cross-section

internal forces and moments:  $T_t = 315.00 \text{ kNcm}$ ,  $T_\omega = 135.00 \text{ kNcm}$

##### 2.1.1. elastic verification

elastic verification for  $T_t = 3.15 \text{ kNm}$ ,  $T_\omega = 1.35 \text{ kNm}$

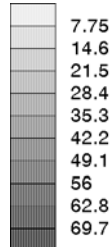
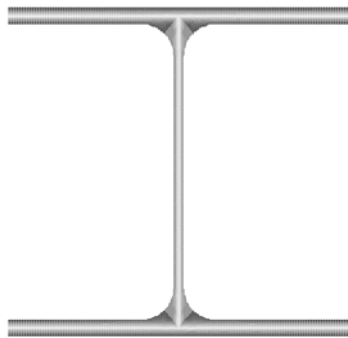
elastic stresses:  $\max |\sigma_x| = 0.00 \text{ N/mm}^2$ ,  $\max \tau = 77.48 \text{ N/mm}^2$ ,  $\max \sigma_v = 134.20 \text{ N/mm}^2$

$\max \sigma_v$  bei  $y = 0.0 \text{ mm}$ ,  $z = -125.0 \text{ mm}$ :  $\sigma_x = 0.00 \text{ N/mm}^2$ ,  $\tau = -77.48 \text{ N/mm}^2$ ,  $\sigma_v = 134.20 \text{ N/mm}^2$

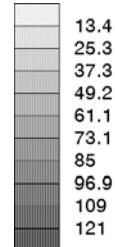
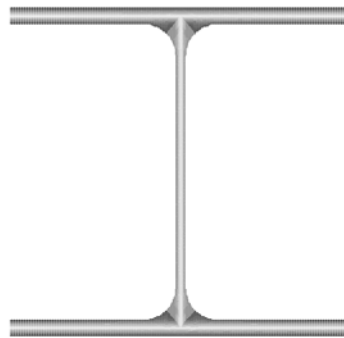
valid equivalent stress:  $\sigma_{v,Rd} = 235.0 \text{ N/mm}^2$

verification:  $\sigma_v = 134.20 \text{ N/mm}^2 < \sigma_{v,Rd} = 235.00 \text{ N/mm}^2 \Rightarrow U_\sigma = 0.571 < 1$  **ok**

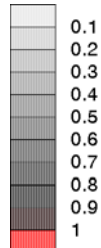
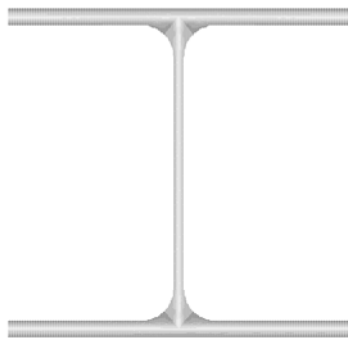
shear stresses  $\tau$  [N/mm<sup>2</sup>]  
max  $\tau$  = 77.5



equivalent stresses  $\sigma_v$  [N/mm<sup>2</sup>]  
max  $\sigma_v$  = 134.2



utilization  $U_\sigma$   
max  $U_\sigma$  = 0.571



stresses, utilizations

| y<br>mm | z<br>mm | $\tau$<br>N/mm <sup>2</sup> | $\sigma_v$<br>N/mm <sup>2</sup> | $U_\sigma$ |
|---------|---------|-----------------------------|---------------------------------|------------|
| -130.0  | 0.0     | 77.48                       | 134.20                          | 0.571      |

y,z: node coordinates;  $\tau, \sigma_v$ : stresses;  $U_\sigma$ : stress utilization

### 3. Lk 2: Stelle 2

#### 3.1. verification of cross-section

internal forces and moments:  $T_\omega = 450.00$  kNm,  $B = 68700.00$  kNcm<sup>2</sup>

##### 3.1.1. elastic verification

elastic verification for  $T_\omega = 4.50$  kNm,  $B = 6.87$  kNm<sup>2</sup>

elastic stresses: max  $|\sigma_x| = 205.37$  N/mm<sup>2</sup>, max  $\tau = 8.74$  N/mm<sup>2</sup>, max  $\sigma_v = 205.37$  N/mm<sup>2</sup>

max  $\sigma_x$  bei  $y = 130.0$  mm,  $z = -118.8$  mm:  $\sigma_x = 205.37$  N/mm<sup>2</sup>,  $\tau = 0.00$  N/mm<sup>2</sup>,  $\sigma_v = 205.37$  N/mm<sup>2</sup>

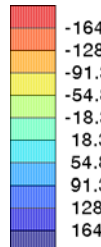
min  $\sigma_x$  bei  $y = -130.0$  mm,  $z = -118.8$  mm:  $\sigma_x = -205.37$  N/mm<sup>2</sup>,  $\tau = 0.00$  N/mm<sup>2</sup>,  $\sigma_v = 205.37$  N/mm<sup>2</sup>

max  $\sigma_v$  bei  $y = 130.0$  mm,  $z = -118.8$  mm:  $\sigma_x = 205.37$  N/mm<sup>2</sup>,  $\tau = 0.00$  N/mm<sup>2</sup>,  $\sigma_v = 205.37$  N/mm<sup>2</sup>

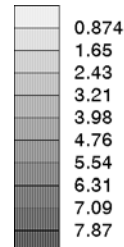
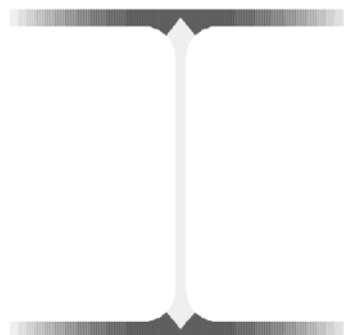
valid equivalent stress:  $\sigma_{v,Rd} = 235.0$  N/mm<sup>2</sup>

verification:  $\sigma_v = 205.37$  N/mm<sup>2</sup> <  $\sigma_{v,Rd} = 235.00$  N/mm<sup>2</sup>  $\Rightarrow U_\sigma = 0.874 < 1$  **ok**

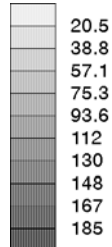
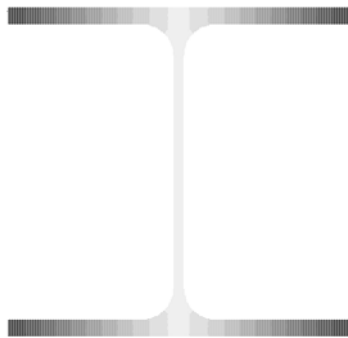
normal stresses  $\sigma_x$  [N/mm<sup>2</sup>]  
min  $\sigma_x = -205.4$ , max  $\sigma_x = 205.4$



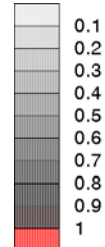
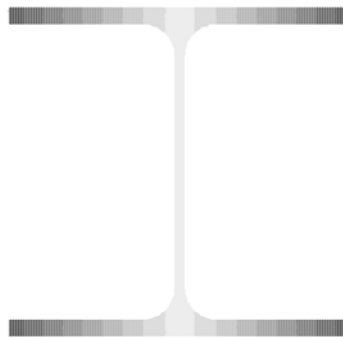
shear stresses  $\tau$  [N/mm<sup>2</sup>]  
max  $\tau$  = 8.7



equivalent stresses  $\sigma_v$  [N/mm<sup>2</sup>]  
max  $\sigma_v$  = 205.4



utilization  $U_\sigma$   
max  $U_\sigma$  = 0.874



stresses, utilizations

| y<br>mm | z<br>mm | $\sigma_x$<br>N/mm <sup>2</sup> | $\tau$<br>N/mm <sup>2</sup> | $\sigma_v$<br>N/mm <sup>2</sup> | $U_\sigma$ | y<br>mm | z<br>mm | $\sigma_x$<br>N/mm <sup>2</sup> | $\tau$<br>N/mm <sup>2</sup> | $\sigma_v$<br>N/mm <sup>2</sup> | $U_\sigma$ |
|---------|---------|---------------------------------|-----------------------------|---------------------------------|------------|---------|---------|---------------------------------|-----------------------------|---------------------------------|------------|
| 0.0     | 12.5    | 205.41                          | 0.00                        | 205.41                          | 0.874      | -130.0  | 6.3     | 0.00                            | 8.74                        | 15.14                           | 0.064      |
| 0.0     | 6.3     | 205.41                          | 0.00                        | 205.41                          | 0.874      | -260.0  | 0.0     | -205.41                         | 0.00                        | 205.41                          | 0.874      |
| 0.0     | 0.0     | 205.41                          | 0.00                        | 205.41                          | 0.874      |         |         |                                 |                             |                                 |            |

y,z: node coordinates;  $\sigma_x, \tau, \sigma_v$ : stresses;  $U_\sigma$ : stress utilization

#### 4. final result

maximum utilization [Lk 2]: resistance max  $U = 0.874 < 1$  **ok**

**verification succeeded**