

# POS. 13: FIRE DESIGN BSP.5.7B

verification of stability EC 3-1-2 (12.10), NA: Deutschland

4H-EC3ST version: 12/2021-1b

## 1. input data

### 1.1. general information

verifications of stability in case of fire acc. to EN 1993-1-2  
lateral torsional buckling with the method of fictitious bars for  $M_y$

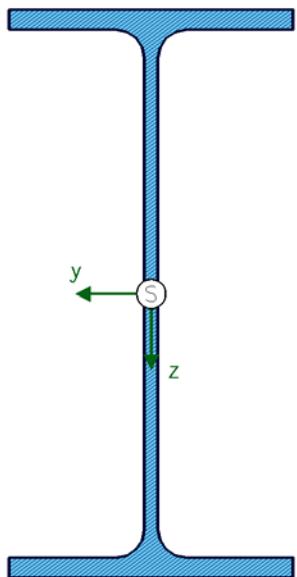
### 1.2. safety factor of material

resistance of cross-sections  $\gamma_{M0} = 1.00$   
resistance of members in stability failure  $\gamma_{M1} = 1.10$   
resistance of components in the event of fire  $\gamma_{M,fi} = 1.00$

### 1.3. cross-section

material: S235 (St37) ( $E = 210000 \text{ N/mm}^2$ ,  $G = 80769 \text{ N/mm}^2$ ,  $f_{y,k} = 235 \text{ N/mm}^2$ )  
section: IPE300

section scale 1:4.0



### 1.4. cross-section values (related to the centre of gravity S)

$I_y = 8360.0 \text{ cm}^4$ ,  $I_z = 604.0 \text{ cm}^4$ ,  $I_{\zeta} = 8360.0 \text{ cm}^4$ ,  $I_{\eta} = 604.0 \text{ cm}^4$ ,  $\alpha = 0.0^\circ$   
 $I_o = 125900.0 \text{ cm}^6$ ,  $I_T = 20.2 \text{ cm}^4$   
 $W_y = 557.0 \text{ cm}^3$ ,  $W_z = 80.5 \text{ cm}^3$ ,  $W_{pl,y} = 628.0 \text{ cm}^3$ ,  $W_{pl,z} = 125.0 \text{ cm}^3$   
 $Z_{m,y} = 0.0 \text{ mm}$ ,  $Z_{m,z} = -0.0 \text{ mm}$ ,  $A = 53.8 \text{ cm}^2$

### 1.5. load application point (related to the center of the surrounding rectangle)

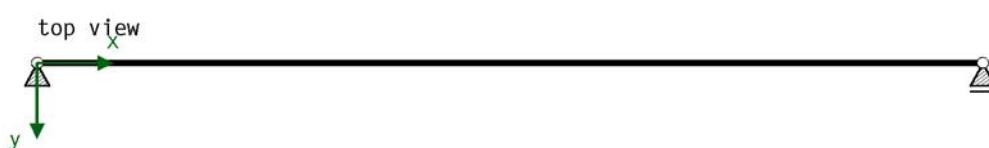
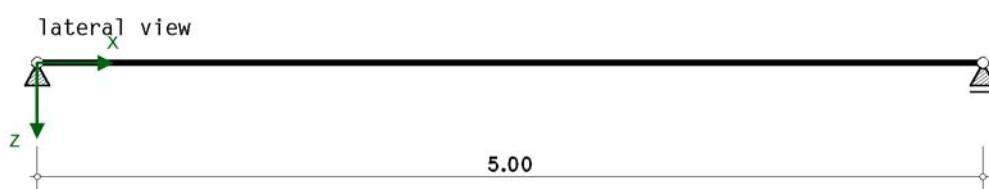
$y_{load} = 0.0 \text{ mm}$  (centroid)

$Z_{load} = -0.0 \text{ mm}$  (shear center)

### 1.6. static system

all bearings with fork restraint, bar length 5.000 [m]

no intermediate bearing in z-direction, no intermediate bearing in y-direction



## 1.7. buckling coefficients

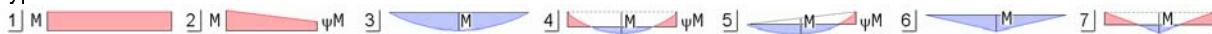
$\perp$  y-axis:  $\beta_y = 1.000$ ,  $\perp$  z-axis:  $\beta_z = 1.000$   
warping restraint intensity  $\beta_0 = 1.000$

## 1.8. design member forces (load combinations)

Lk	type $\perp y$	$M_{0y,d}$ kNm	$\psi_y$	$k_{c,y}$	$\zeta_y$
1	3	39.00	0.000	0.940	1.128

type (y): type of moment curves each direction;  $M_{0y,d}, \psi_y$ : reference values of moment curve;  $k_{c,y}, \zeta_y$ : coefficients for calculation

types of moment curves



## 1.9. fire design

thermal action due to the standard curve, fire resistance time  $t = 10.7$  min

emissivity of the cross-section surface of untreated steel

section all sides flamed

maximum density steel 7850.0 kg/m³, room temperature 20.0 °C

fire design at load level

adjustment factors of bending moments for uneven temperature distribution

across the cross section  $\kappa_1 = 1.00$ , along the beam  $\kappa_2 = 1.00$

## 2. cross-section temperature

surface of the section exposed to fire  $A_m = 1160.0 \text{ mm}^2/\text{mm}$

section factor of the unprotected component  $A_m/V = 1160.0 / 5381.2 \cdot 10^3 = 215.6 \text{ 1/m}$

fire-stressed inner surface of the enclosing box  $A_b = 900.0 \text{ mm}^2/\text{mm}$

section factor for the enclosing box  $A_b/V = 900.0 / 5381.2 \cdot 10^3 = 167.2 \text{ 1/m}$

correction factor  $k_{sh} = (A_b/V) / (A_m/V) = 167.2 / 215.6 = 0.776$ , I-section:  $0.9 \cdot k_{sh} = 0.698$

cross-section temperature acc. to  $t = 10.7$  min:  $T_a = 518.6 \text{ °C}$

reduction factors:  $k_{y,fi} = 0.722$ ,  $k_{E,fi} = 0.546$

material parameters:  $f_y,fi = 169.8 \text{ N/mm}^2$ ,  $E_{fi} = 114674.7 \text{ N/mm}^2$

## 3. verifications

### 3.1. classification of cross-section

#### 3.1.1. load combination 1 $\Rightarrow$ section class 1

no	c mm	t mm	c/t	$\epsilon$	$\sigma_1$ N/mm²	$\sigma_2$ N/mm²	tab 5.2	$\alpha$	$\psi$	$k_\sigma$	class
1	56.5	10.7	5.28	0.850	67.48	67.48	single 1/1	---	---	---	1
2	56.5	10.7	5.28	0.850	67.48	67.48	single 1/1	---	---	---	1
3	248.6	7.1	35.01	0.850	57.99	-57.99	both 1/1	---	---	---	1
4	56.5	10.7	5.28	1.177	-67.48	-67.48	-----	---	---	---	---
5	56.5	10.7	5.28	1.177	-67.48	-67.48	-----	---	---	---	---

compressive stresses have a positive sign acc. to EC 3.

classification of cross-section in case of fire acc. to EC 3-1-2, 4.2.2.

the verifications are carried out in the smallest possible cross-section class 1

### 3.2. lateral torsional buckling for bending around y-axis

$c^2 = 53427 \text{ mm}^2$ , buckling curve 'fire'  $\Rightarrow \alpha_{LT} = 0.65$ ,  $N_{cr} = 273.44 \text{ kN}$

#### 3.2.1. utilisations

event of fire:  $M_{Ed} = \kappa_1 \cdot \kappa_2 \cdot M_{Ed}$

Lk	class	$M_{cr}$ kNm	$\lambda_{LT}$	f	$\Phi_{LT}$	$\chi_{LT}$ m	$\chi_{LT,mod}$ m	$M_{Ed}$ kNm	$M_{b,Rd}$ kNm	U
1	$1 \Rightarrow W_{p1,y}$	71.30	1.223	1.000	1.645	0.364	0.364	39.00	38.83	1.004

max U = 1.004 > 1 **not ok !!**

## 4. final result

maximum utilisation  $U = 1.004 > 1$  **not ok !!**

**resistance not ensured !!**

## 5. Selected Design Parameters of the National Annex

DIN EN 1993-1-1 (EC 3, Hochbau), NA Deutschland

chapter	value	definition
6.1(1)	permanent/transient situation $\gamma_{M0} = 1.00$ $\gamma_{M1} = 1.10$ $\gamma_{M2} = 1.25$	partial safety factors for structural steel collapse of cross-section instability fracture cross-sections in tension
	accidental situation $\gamma_{M0} = 1.00$ $\gamma_{M1} = 1.00$ $\gamma_{M2} = 1.25$	partial safety factors for structural steel collapse of cross-section instability fracture cross-sections in tension
6.3.2.2(2)	factor f to modify $\chi_{LT}$	lateral torsional buckling general case
6.3.2.3(1)	$\lambda_{LT,0} = 0.40$	slenderness eqn. (6.75)
6.3.2.3(2)	$\beta = 0.75$	correction factor eqn. (6.75)
	coefficient $k_c$ from tab. 6.6	calculation of the reduction factor $\chi_{LT}$

DIN EN 1993-1-2 (EC 3, Brandfall), NA Deutschland

chapter	value	definition
2.3(1)	event of fire $\gamma_{M,f1} = 1.00$	partial safety factor for mechanical failure