

1. input data

1.1. general information

verifications of stability in case of fire acc. to EN 1993-1-2
flexural buckling with the method of fictitious bars, buckling only in y-direction

1.2. safety factor of material

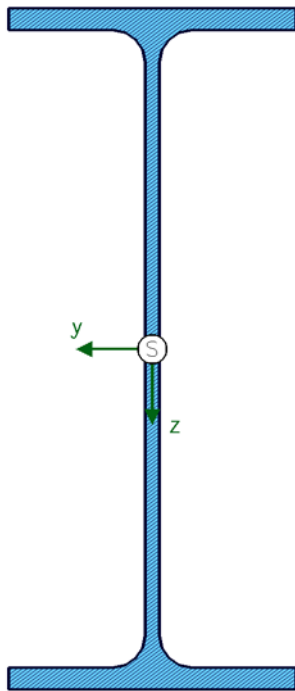
resistance of cross-sections $\gamma_{M0} = 1.00$
resistance of members in stability failure $\gamma_{M1} = 1.10$
resistance of components in the event of fire $\gamma_{M,fi} = 1.00$

1.3. cross-section

material: S235 (St37) ($E = 210000 \text{ N/mm}^2$, $G = 80769 \text{ N/mm}^2$, $f_{y,k} = 235 \text{ N/mm}^2$)

section: IPE450

section scale 1:5.0



1.4. cross-section values (related to the centre of gravity S)

$I_y = 33740.0 \text{ cm}^4$, $I_z = 1680.0 \text{ cm}^4$, $I_{yz} = 33740.0 \text{ cm}^4$, $I_{\eta} = 1680.0 \text{ cm}^4$, $\alpha = 0.0^\circ$

$I_{\omega} = 791000.0 \text{ cm}^6$, $I_T = 67.1 \text{ cm}^4$

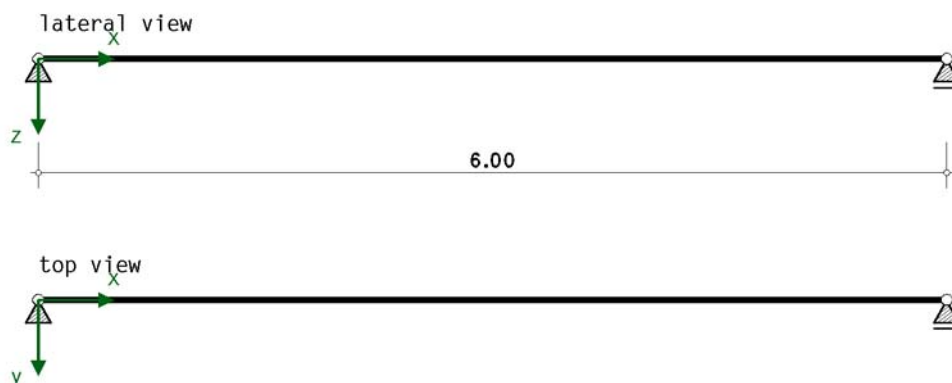
$W_y = 1500.0 \text{ cm}^3$, $W_z = 176.0 \text{ cm}^3$, $W_{pl,y} = 1702.0 \text{ cm}^3$, $W_{pl,z} = 275.0 \text{ cm}^3$

$z_{m,y} = 0.0 \text{ mm}$, $z_{m,z} = 0.0 \text{ mm}$, $A = 98.8 \text{ cm}^2$

1.5. static system

all bearings with fork restraint, bar length 6.000 [m]

no intermediate bearing in z-direction, no intermediate bearing in y-direction



1.6. buckling coefficients

⊥ y-axis: $\beta_y = 1.000$, ⊥ z-axis: $\beta_z = 1.000$

warping restraint intensity $\beta_0 = 1.000$

1.7. design member forces (load combinations)

Lk	N _d kN
1	136.50

N_d: constant axial force in the bar

1.8. fire design

thermal action due to the standard curve, fire resistance time $t = 15.0$ min

emissivity of the cross-section surface of untreated steel steel

section all sides flamed

maximum density steel 7850.0 kg/m^3 , room temperature 20.0 °C

fire design at load level

adjustment factors of bending moments for uneven temperature distribution

across the cross section $\kappa_1 = 1.00$, along the beam $\kappa_2 = 1.00$

2. cross-section temperature

surface of the section exposed to fire $A_m = 1605.1 \text{ mm}^2/\text{mm}$

section factor of the unprotected component $A_m/V = 1605.1 / 9882.1 \cdot 10^3 = 162.4 \text{ 1/m}$

fire-stressed inner surface of the enclosing box $A_b = 1280.0 \text{ mm}^2/\text{mm}$

section factor for the enclosing box $A_b/V = 1280.0 / 9882.1 \cdot 10^3 = 129.5 \text{ 1/m}$

correction factor $k_{sh} = (A_b/V) / (A_m/V) = 129.5 / 162.4 = 0.797$, I-section: $0.9 \cdot k_{sh} = 0.718$

cross-section temperature acc. to $t = 15.0$ min: **$T_a = 598.9 \text{ °C}$**

reduction factors: $k_{y,fi} = 0.473$, $k_{E,fi} = 0.313$

material parameters: $f_{y,fi} = 111.3 \text{ N/mm}^2$, $E_{fi} = 65770.4 \text{ N/mm}^2$

3. verifications

3.1. classification of cross-section

3.1.1. load combination 1 ⇒ section class 1

no	c mm	t mm	c/t -	ε -	σ ₁ N/mm ²	σ ₂ N/mm ²	tab 5.2	α -	ψ -	k _σ -	class -
1	69.3	14.6	4.75	0.850	13.82	13.82	single 1/1	---	---	---	1
2	69.3	14.6	4.75	0.850	13.82	13.82	single 1/1	---	---	---	1
3	378.8	9.4	40.30	0.850	13.82	13.82	both 2/0	---	---	---	4
4	69.3	14.6	4.75	0.850	13.82	13.82	single 1/1	---	---	---	1
5	69.3	14.6	4.75	0.850	13.82	13.82	single 1/1	---	---	---	1

compressive stresses have a positive sign acc. to EC 3.

classification of cross-section in case of fire acc. to EC 3-1-2, 4.2.2.

verifications are carried out in the **specified** cross-section class 1

buckling of the individual sheets of the cross-section is to be veriflicated separately !!

3.2. flexural buckling and torsional buckling

$\lambda_y = 0.425 < \lambda_T = 1.905 \Rightarrow$ torsional buckling (λ_T) decisive

$\lambda_z = 1.905 < \lambda_T = 1.905 \Rightarrow$ torsional buckling (λ_T) decisive

$I_p = 35420 \text{ cm}^4$, $I_T = 67 \text{ cm}^4$, $i_p^2 = 35850 \text{ mm}^2$, $c^2 = 103116 \text{ mm}^2$, $i_m^2 = 35850 \text{ mm}^2$

flexural buckling around y-axis:

$i_y = 184.8 \text{ mm}$, $\beta_z = 1.00$ (⊥ z-axis), $L_{cr,z} = 6.000 \text{ m}$, $\lambda_1 = 76.386$

$\lambda_y = 1.905$, y-buckling curve 'fire' $\Rightarrow \alpha_y = 0.65$, $\Phi_y = 2.933$, $\chi_y = 0.194$, **$N_{by,Rd} = 212.85 \text{ kN}$**

flexural buckling around z-axis:

$i_z = 41.2 \text{ mm}$, $\beta_y = 1.00$ (⊥ y-axis), $L_{cr,y} = 6.000 \text{ m}$, $\lambda_1 = 76.386$

$\lambda_z = 1.905$, z-buckling curve 'fire' $\Rightarrow \alpha_z = 0.65$, $\Phi_z = 2.933$, $\chi_z = 0.194$, **$N_{bz,Rd} = 212.85 \text{ kN}$**

3.2.1. utilisations

Lk	N _d kN	U _y -	U _z -
1	136.50	0.641	0.641

max U = **0.641** < 1 **ok**

4. final result

maximum utilisation $U = 0.641 < 1$ **ok**

verification succeeded

5. Selected Design Parameters of the National Annex

DIN EN 1993-1-1 (EC 3, Hochbau), NA Deutschland

chapter	value	definition
6.1(1)	permanent/transient situation	partial safety factors for structural steel
	$\gamma_{M0} = 1.00$	collapse of cross-section
	$\gamma_{M1} = 1.10$	instability
	$\gamma_{M2} = 1.25$	fracture cross-sections in tension
	accidental situation	partial safety factors for structural steel
	$\gamma_{M0} = 1.00$	collapse of cross-section
	$\gamma_{M1} = 1.00$	instability
	$\gamma_{M2} = 1.25$	fracture cross-sections in tension
6.3.2.2(2)	factor f to modify	lateral torsional buckling
	χ_{LT}	general case
6.3.2.3(1)	$\lambda_{LT,0} = 0.40$	slenderness eqn. (6.75)
	$\beta = 0.75$	correction factor eqn. (6.75)
6.3.2.3(2)	coefficient k_c from tab. 6.6	calculation of the reduction factor χ_{LT}

DIN EN 1993-1-2 (EC 3, Brandfall), NA Deutschland

chapter	value	definition
2.3(1)	event of fire	partial safety factor for
	$\gamma_{M,f1} = 1.00$	mechanical failure