

1. input data

1.1. general settings

vibration analysis in accordance with the design and dimensioning rules from the research project Winter/Hamm/Richter: "Schwingungs- und Dämpfungsverhalten von Holz- und Holz-Beton-Verbunddecken" TU München 2010

ceiling between different utilisation units $\Rightarrow f_{\text{grenz}} = 8 \text{ Hz}$, $w_{\text{grenz}} = 0.5 \text{ mm}$, $a_{\text{grenz}} = 0.70 \text{ m/s}^2$

modal damping ratio $\xi = 0.01$

continuous effect is not taken into account in the stiffness criterion

calculation using approximation formulas acc. to DIN EN 1995-1-1, 7.3.3

1.2. dimensions

ceiling width $b = 3.500 \text{ m}$, 3 span(s), all outer edges are hinged

span	l m
1	4.600
2	3.450
3	4.500

continuous effect is not taken into account in the stiffness criterion

all intermediate support axles are rigidly mounted

1.3. permanent action effects

Nr.	action eff	g kN/m ²
1	permanent loads	0.838
Σ		0.838

1.4. screed

60 mm cement screed, $E = 25000 \text{ N/mm}^2$, $g = 1.320 \text{ kN/m}^2$, $I_{\text{screed}} = 18000000 \text{ mm}^4/\text{m}$

$\Rightarrow EI_{\text{screed}} = 450.000000 \text{ Mm}^2/\text{m}$

with consideration of rigidity in the transverse direction as well

1.5. cross laminated timber ceiling panel

Merkle X-Lam 180/5s, structure **40.0-30.0-40.0-30.0-40.0** solid coniferous timber C24

top layers in x-direction, $d = 180.0 \text{ mm}$

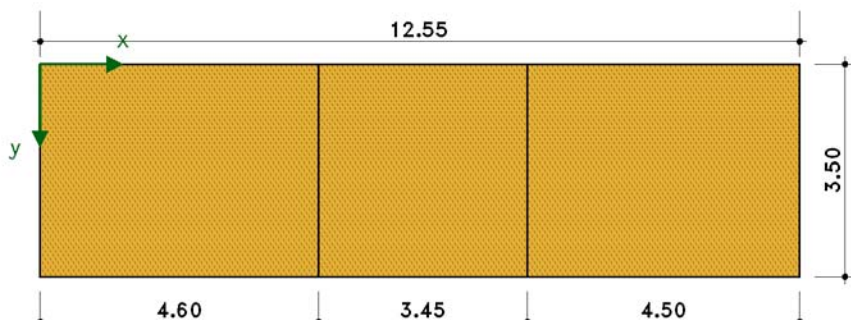
without consideration of shear deformations in x-direction

without consideration of shear deformations in y-direction

lateral contraction number $\nu = 0.00$, drill stiffness = 50.0

plate is clamped with 2- axis

1.6. plan view scale 1:125



2. results

2.1. natural frequency

Attention! All stiffnesses are user-defined!

$EI_{\text{lengthwise}} = 3.038000 \text{ MNm}^2/\text{m}$, $EI_{\text{cross}} = 0.871000 \text{ MNm}^2/\text{m}$

$k_f = 1.175$, $b_{ef} = 3.060$, $\alpha = 1.040 \Rightarrow f(\alpha) = 1.362$, $m = 220.0 \text{ kg/m}^2$

$f_e = 13.966 \text{ Hz} \geq f_e = 8 \text{ Hz} \Rightarrow$ **criterion fulfilled!**

2.2. stiffness criterion

$b_{ef} = 3.060 \text{ m}$

$w(2\text{kN}) = 0.23 \text{ mm} \leq w_{\text{grenz}} = 0.5 \text{ mm} \Rightarrow$ **criterion fulfilled!**

2.3. constructive requirements

floating storage of the screed is absolutely necessary!

acc. to [Winter/Hamm/Richter], TU München 2010 gilt:

Due to their higher mass and greater rigidity, wet screeds are better than dry screeds in terms of the vibration behaviour of the ceilings.

A (preferably heavy) fill improves the vibration behaviour.

The heavier the fill, the greater the improvement in the subjective assessment.

Heavy fills are fills with a surface weight of at least 60 kg/m².

verification fulfilled!