

1. Options for Calculations

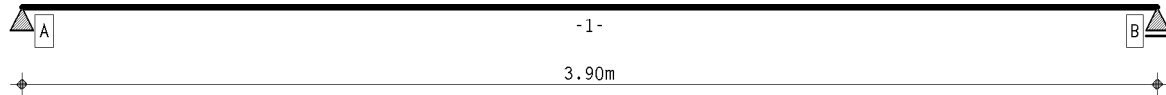
calculation DIN EN 1995:2010, Germany

service class 2

coefficient of thermal expansion for timber $\alpha_t = 0.500 \cdot 10^{-5}/^{\circ}\text{K}$

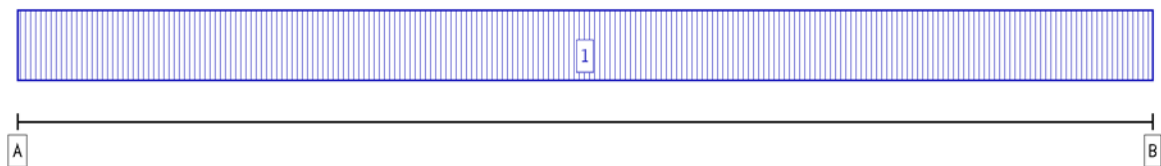
$\psi_2 = 0.60$ (factor acc. to DIN EN 1995-1-1 2.3.2.2 (2))

2. Structural system

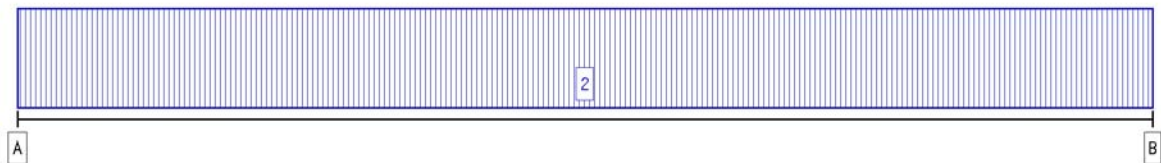


main beam

3. Loading



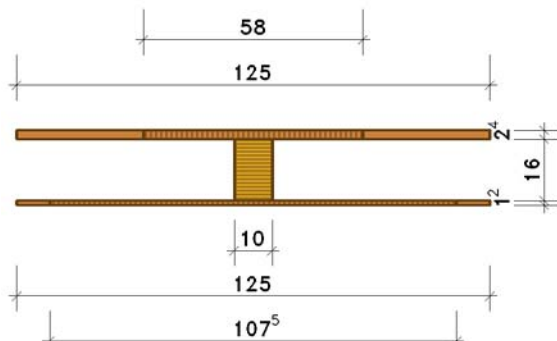
action effect 1: permanent loads (permanent, 1 load cases)



action effect 2: live loads (1) (transient, 1 load cases)

4. main beam

section scale 1:20



timber gr. top fl. (fibre II) plywood F25/10

d = 24.0 mm (lying)

char. bend. strength $f_{m,k}$: 25.0 N/mm²

char. shear strength $f_{v,k}$: 1.1 N/mm²

char. ten. strength $f_{t,k}$: 18.0 N/mm²

char. compr. strength $f_{c,0,k}$: 18.0 N/mm²

char. compr. strength $f_{c,90,k}$: 6.5 N/mm²

e-modulus $E_{0,mean}$ (diaphragm): 4500 N/mm²

e-modulus $E_{0,mean}$ (plate) : 5500 N/mm²

Dichte ρ_k/ρ_m : 400 / 480 kg/m³

deformation factor k_{def} : 1.00 -

area A_{flange} : 300.000 cm²

moment of inertia I_{flange} : 144.000 cm⁴

timber grade web solid coniferous timber, C24 (S10)

char. bend. strength $f_{m,k}$: 24.0 N/mm²

char. shear strength $f_{v,k}$: 4.0 N/mm²

char. ten. strength $f_{t,k}$: 14.5 N/mm²

char. compr. strength $f_{c,0,k}$: 21.0 N/mm²

char. compr. strength $f_{c,90,k}$: 2.5 N/mm²

k_{cr} : 0.50 mm²/N

modulus of elasticity $E_{0,mean}$: 11000 N/mm²

Dichte ρ_k/ρ_m : 350 / 420 kg/m³

deformation factor k_{def} : 0.80 -

area A_{flange} : 160.000 cm²

moment of inertia I_{flange} : 3413.333 cm⁴

timber grade bottom flange (fibre II) OSB 2

d = 12.0 mm (lying)

char. bend. strength $f_{m,k}$: 16.4 N/mm²

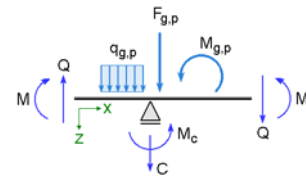
char. shear strength $f_{v,k}$: 1.0 N/mm²

char. ten. strength $f_{t,k}$: 9.4 N/mm²

char. compr. strength $f_{c,0,k}$: 15.4 N/mm²

char. compr. strength $f_{c,90,k}$: 10.0 N/mm²

e-modulus $E_{0,\text{mean}}$ (diaphragm): 3800 N/mm²
e-modulus $E_{0,\text{mean}}$ (plate): 4930 N/mm²
Dichte ρ_k/ρ_m : 550 / 660 kg/m³
deformation factor k_{def} : 2.25 -
area A_{flange} : 150.000 cm²
moment of inertia I_{flange} : 18.000 cm⁴
definition of internal forces and moments:



5. Beam sections

beam sections

section	x_A m	x_E m	l m	l_{ef} m	l_z mm	k -	λ -	$\lambda_{\text{rel,c}}$ -	k_c -	l_v m	cant11.	s_{ef} mm
1	0.00	3.90	3.90	2.00	28.9000	1.2827	69.2042	1.1788	0.5592	3.90	-	n.e.

stiffness values serviceability initial state

section	γ_2 -	a_2 mm	K_1 N/mm	γ_{1r} -	a_1 mm	K_3 N/mm	γ_3 -	a_3 mm	$E I_{\text{ef,inst}}$ Nmm ²	ϕ k_{def} -
1	1.0000	-5.4	1	1.0000	-86.6	1	1.0000	91.4	1.2670E12	0.7467

stiffness values load-carrying capacity initial state

section	γ_2 -	a_2 mm	K_1 N/mm	γ_1 -	a_1 mm	K_3 N/mm	γ_3 -	a_3 mm	$E I_{\text{ef,inst}}$ Nmm ²	$I_{\text{ef,inst}}$ mm ²	$h_{q,\text{inst}}$ mm	$A_{q,\text{inst}}$ mm
1	1.0000	-5.4	1	1.0000	-86.6	1	1.0000	91.4	1.2670E12	115186024.0	8.54	106.67

stiffness values load-carrying capacity final state

section	γ_2 -	a_2 mm	K_1 N/mm	γ_1 -	a_1 mm	K_3 N/mm	γ_3 -	a_3 mm	$E I_{\text{ef,inf}}$ Nmm ²	$I_{\text{ef,inf}}$ mm ²	$h_{q,\text{inf}}$ mm	$A_{q,\text{inf}}$ mm
1	1.0000	-10.1	1	1.0000	-81.9	1	1.0000	96.1	7.2541E11	97600776.00	9.01	106.67

net section properties

section	$A_{n,2}$ cm ²	$W_{n,2}$ cm ³	$I_{n,2}$ cm ⁴	$A_{n,1}$ cm ²	$W_{n,1}$ cm ³	$I_{n,1}$ cm ⁴	$A_{n,3}$ cm ²	$W_{n,3}$ cm ³	$I_{n,3}$ cm ⁴
1	160.00	426.67	3413.33	139.20	120.00	144.00	129.00	30.00	18.00

6. Fasteners

section 1 from $x_A = 0.00$ m to $x_E = 3.90$, glued joint

7. Supports

coordinates of supports

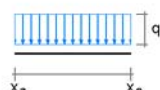
supp.name	x m	width mm	depth mm	cF kN/m	CM kNm/-	restraint (F) (M)
A	0.00	150	1250	fix	----	X -
B	3.90	150	1250	fix	----	X -

8. Action effects

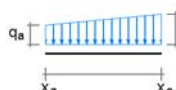
Attention! Acc. to DIN EN 1995-1-1, annex B.1

mechanically jointed cross-sections are only allowed to be loaded by line loads

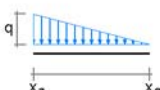
uniformly distributed load



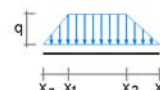
trapezoidal load



triangular load



trapezoidal load (spec.)



dead load



temperature



point load/ moment



displacement of support



Permanent action effect: permanent loads

1. additive load case: dead load (1)

→ unif.distr.load: $q = 2.00$ kN/m from $x_a = 0.00$ m to $x_e = 3.90$ m

2. Transient action effect: live loads (1)

2. additive load case: live loads (1/1)

→ unif.distr.load: $q = 2.20$ kN/m from $x_a = 0.00$ m to $x_e = 3.90$ m

9. verifications

1: EC 5 load-carrying capacity

buckling analysis of compression flange acc. to DIN EN 1995, 6.3.2 will be executed

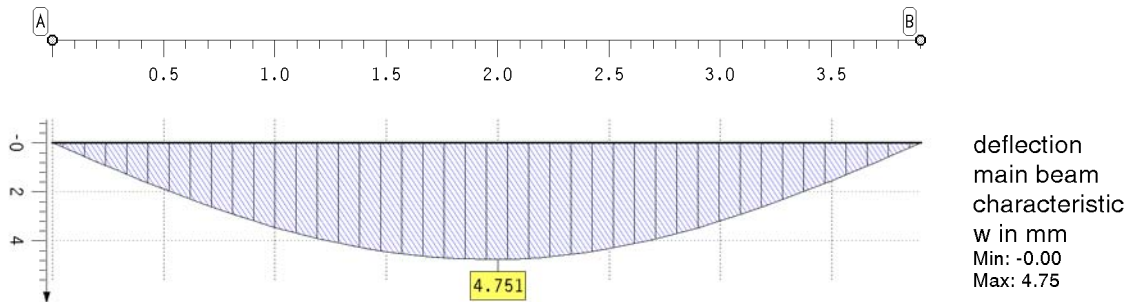
verification of bearing stress DIN EN 1995, 6.1.5 will be executed

Extreme rule 1

10. Results of action effects

10.1. Action effect 1: permanent loads

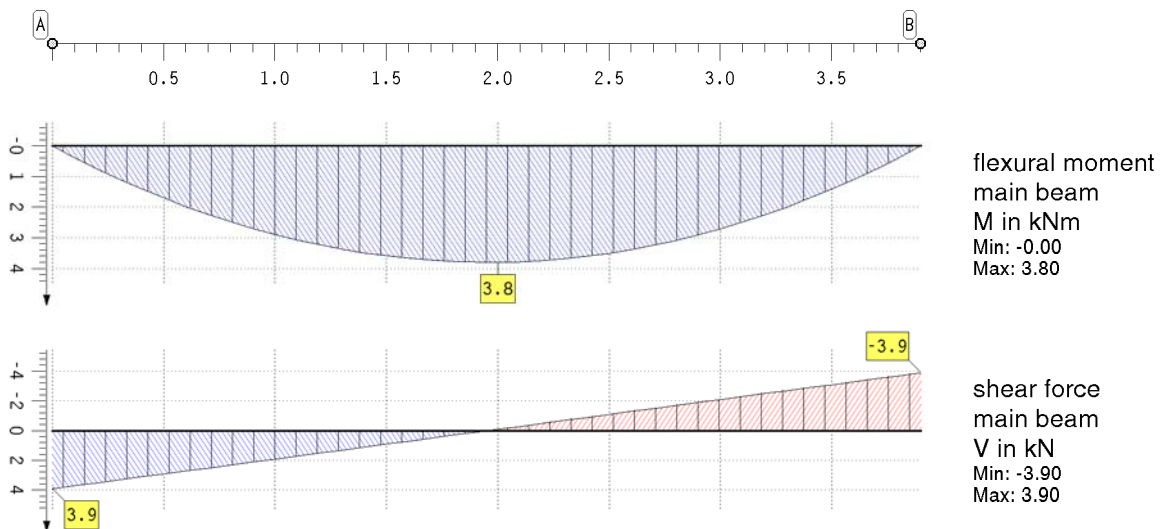
extremal deflections of main beam (characteristic)



extremal deflections of main beam (characteristic)

point	x	min w	max w	point	x	min w	max w
-	m	mm	mm	-	m	mm	mm
A	0.000	0.00	0.00	B	3.900	-0.00	-0.00
	1.100	3.71	3.71	minimum		-0.00	-0.00
	1.900	4.75	4.75	maximum		4.75	4.75
	2.800	3.71	3.71				

extremal internal forces



extremal internal forces

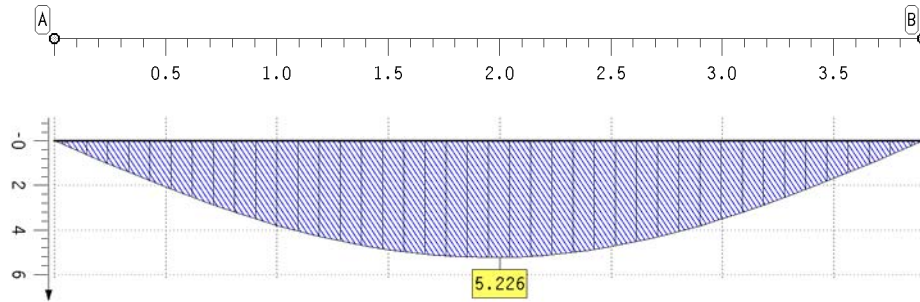
point	x	min M	max M	min V	max V	point	x	min M	max M	min V	max V
-	m	kNm	kNm	kN	kN	-	m	kNm	kNm	kN	kN
A	0.000	0.00	0.00	3.90	3.90	B	3.900	-0.00	-0.00	-3.90	-3.90
	1.000	2.90	2.90	1.90	1.90	minimum		-0.00	-0.00	-3.90	-3.90
	1.900	3.80	3.80	0.10	0.10	maximum		3.80	3.80	3.90	3.90
	2.900	2.90	2.90	-1.90	-1.90						

extremal support forces

point	x	min AP	max AP
-	m	kN	kN
A	0.000	-3.90	-3.90
B	3.900	-3.90	-3.90

10.2. Action effect 2: live loads (1)

extremal deflections of main beam (characteristic)

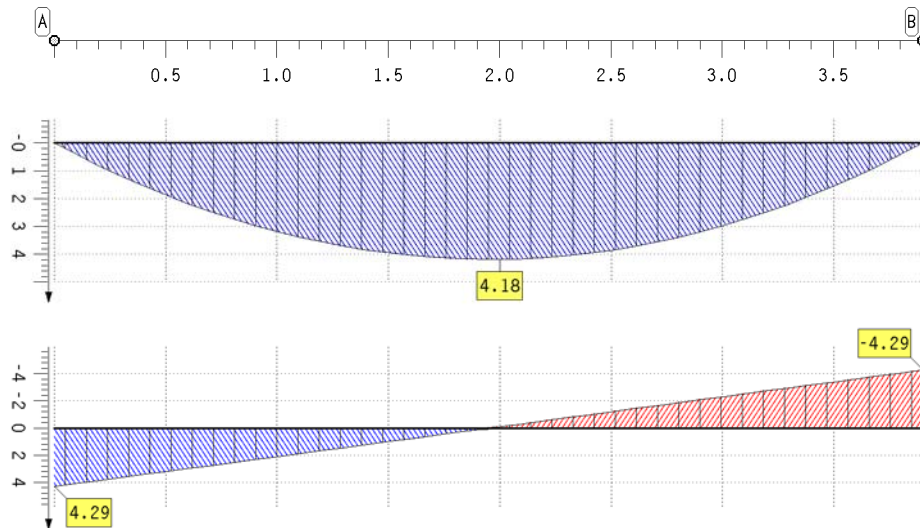


deflection
main beam
characteristic
w in mm
Min: 0.00
Max: 5.23

extremal deflections of main beam (characteristic)

point	x	min w	max w	point	x	min w	max w
-	m	mm	mm	-	m	mm	mm
A	0.000	0.00	0.00	B	3.900	0.00	0.00
	1.100	0.00	4.08	minimum		0.00	0.00
	1.900	0.00	5.23	maximum		0.00	5.23
	2.800	0.00	4.08				

extremal internal forces



flexural moment
main beam
M in kNm
Min: -0.00
Max: 4.18

shear force
main beam
V in kN
Min: -4.29
Max: 4.29

extremal internal forces

point	x	min M	max M	min V	max V	point	x	min M	max M	min V	max V
-	m	kNm	kNm	kN	kN	-	m	kNm	kNm	kN	kN
A	0.000	0.00	0.00	0.00	4.29	B	3.900	-0.00	-0.00	-4.29	-0.00
	1.000	0.00	3.19	0.00	2.09	minimum		-0.00	0.00	-4.29	-0.00
	1.900	0.00	4.18	0.00	0.11	maximum		0.00	4.18	0.00	4.29
	2.900	0.00	3.19	-2.09	-0.00						

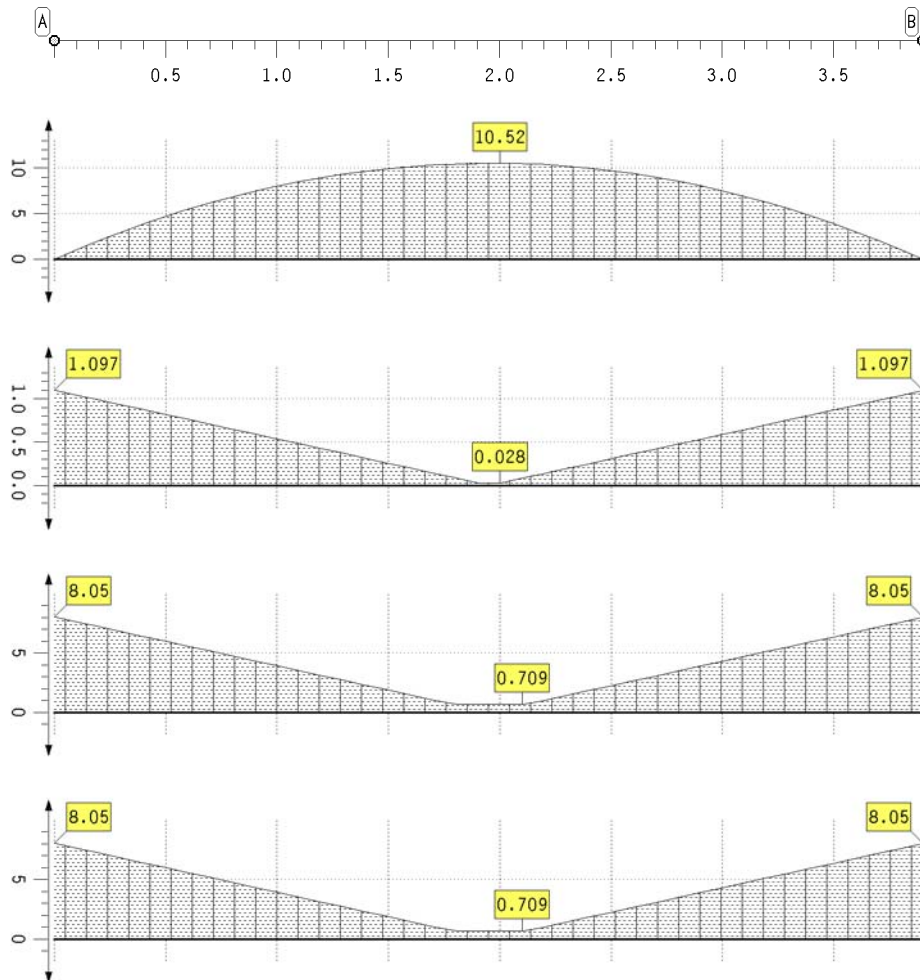
extremal support forces

point	x	min AP	max AP
-	m	kN	kN
A	0.000	-4.29	-0.00
B	3.900	-4.29	-0.00

11. Results of verification of ultimate limit state

11.1. Verification of ultimate limit state

results of verification of ultimate limit state



bending stress
main beam
 σ_h in MN/m²
Max: 10.52

shear stress
main beam
 τ_h in MN/m²
Max: 1.10

utilization
main beam
Max: 8.05

maximal
utilization
Max: 8.05

maximal utilization

point	x	U	point	x	U
-	m	-	-	m	-
A	0.000	8.050	B	3.900	8.050
	1.800	0.709	minimum		0.709
	2.200	1.032	maximum		8.050

extremal support forces

point	x	min AP	max AP
-	m	kN	kN
A	0.000	-11.70	-3.90
B	3.900	-11.70	-3.90

verification of bearing stress

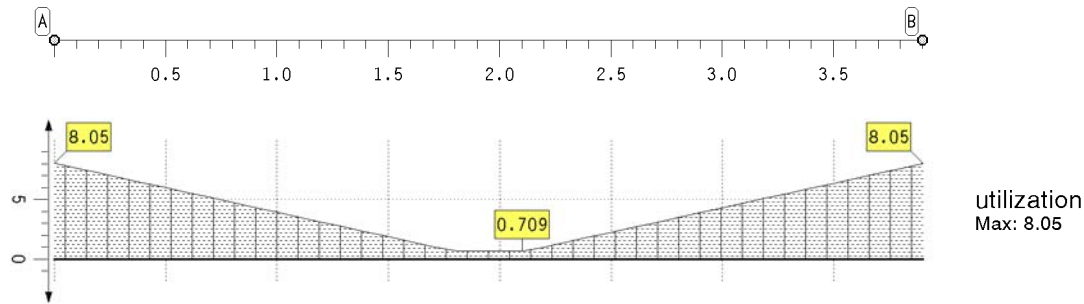
support	l_{ef}	A_{ef}	A_P	k_{c90}	k_{mod}	f_{c90d}	σ_{c90d}	u
	mm	mm ²	N		-	N/mm ²	N/mm ²	-
A	180	225000	11700	1.00	1.00	7.69	0.05	0.01
B	180	225000	11700	1.00	1.00	7.69	0.05	0.01

verification of bearing stresses für den main beam(u = 0.007) successful!

12. Summary

12.1. Summary of all verifications

maximal utilization



maximal utilization

point	x	U	point	x	U
-	m	-	-	m	-
A	0.000	8.050	B	3.900	8.050
	1.800	0.709	minimum		0.709
	2.200	1.032	maximum		8.050

verification of bearing stress

support	l_{ef}	A_{ef}	A_p	k_{c90}	k_{mod}	f_{c90d}	σ_{c90d}	u
	mm	mm ²	N	-	-	N/mm ²	N/mm ²	-
A	180	225000	11700	1.00	1.00	7.69	0.05	0.01
B	180	225000	11700	1.00	1.00	7.69	0.05	0.01

verification of bearing stresses für den main beam(u = 0.007) successful!

13. Utilizations of all verifications

verification of load-carrying capacity (u = 8.050) does not meet the requirements!

14. Detailed verification piont

14.1. Verification of load-carrying capacity at x = 0.00 m

internal forces and moments

state	M	V	M ₁	N ₁	M ₂	N ₂	M ₃	N ₃
	kNm	kN	Nmm	N	Nmm	N	Nmm	N
start,min	0.00	3.90	0	-0	0	0	0	0
start,max	0.00	11.70	0	-0	0	0	0	0
end,min	0.00	3.90	0	-0	0	0	0	0
end,max	0.00	11.70	0	-0	0	0	0	0

stresses and utilization web

state	$k_{mod,2}$	$\sigma_{m,2}$	$\sigma_{c,2}$	$u_{\sigma,2}$	τ_2	u_{τ}	u_2
	-	N/mm ²	N/mm ²	-	N/mm ²	-	-
start	0.8	0.00	0.00	0.00	1.10	0.45	0.45
end	0.8	0.00	0.00	0.00	1.10	0.45	0.45

stresses and utilization flanges

state	$k_{mod,1}$	$\sigma_{m,1}$	$\sigma_{c,1}$	u_1	$k_{mod,3}$	$\sigma_{m,3}$	$\sigma_{c,3}$	u_3
	-	N/mm ²	N/mm ²	-	-	N/mm ²	N/mm ²	-
start	0.8	0.00	-0.00	0.00	1.0	0.00	0.00	0.00
end	0.8	0.00	-0.00	0.00	1.0	0.00	0.00	0.00

adhering joint with $f_{v1,d} = 0.400$ N/mm²

state	$S_{1,d}$	$\tau_{1,d}$	$u_{1,d}$	$S_{2,d}$	$\tau_{2,d}$	$u_{2,d}$
	cm ²	N/mm ²	-	cm ²	N/mm ²	-
start	1206	1.3666	3.42	1179	1.4862	1.93
end	1140	1.3666	3.42	1240	1.4862	1.93

resulting utilization at verification point $u_{res} = 8.050$