

SYSTEM DESCRIPTION

General information

The extension of the longitudinal axis of the beam is oriented to the global X-axis.

Dead loads act in global X-direction.

Calculation is carried out taking into account warping torsion and the Wagner effect.

The deformations of the load spectra don't include the imperfections.

At non linear calculation iteration runs through maximal 50 steps per load spectrum.

Convergence criterion: The iteration is stopped if the result differences of two following steps do not exceed at no point the tolerances listed below.

criterion	tolerance	criterion	tolerance
displacements	0.00010 mm	int. forces	0.00010 kN
rotations	0.00010 ‰	int. moments	0.00010 kNm
twists	0.00010 ‰/m	warping bimom.	0.00010 kNm ²

verification options

Results acc. to DIN EN 1993:2010, NA Germany

Limiting values of (c/t) acc. to DIN EN 1993-1-1 table 5.2 are not being checked.

Plastic cross-section verification acc. to DIN EN 1993-1-1 paragraph 6.2.1(6).

The ultimate limit state is determined according to the extended partial section method.

For triple-sheet cross-sections, the partial section sizing method with rearrangement (KINDMANN) is used.

There is no limitation of limiting bending moments.

Regulations

DIN EN 1993-1-1, Eurocode 3: Bemessung und Konstruktion von Stahlbauten -

Teil 1-1: Allgemeine Bemessungsregeln und Regeln für den Hochbau;

Deutsche Fassung EN 1993-1-1:2005 + AC:2009, Ausgabe Dezember 2010

DIN EN 1993-1-1/A1, Ergänzungen zur DIN EN 1993-1-1, Ausgabe Juli 2014

DIN EN 1993-1-1/NA, Nationaler Anhang zur DIN EN 1993-1-1, Ausgabe Dezember 2018

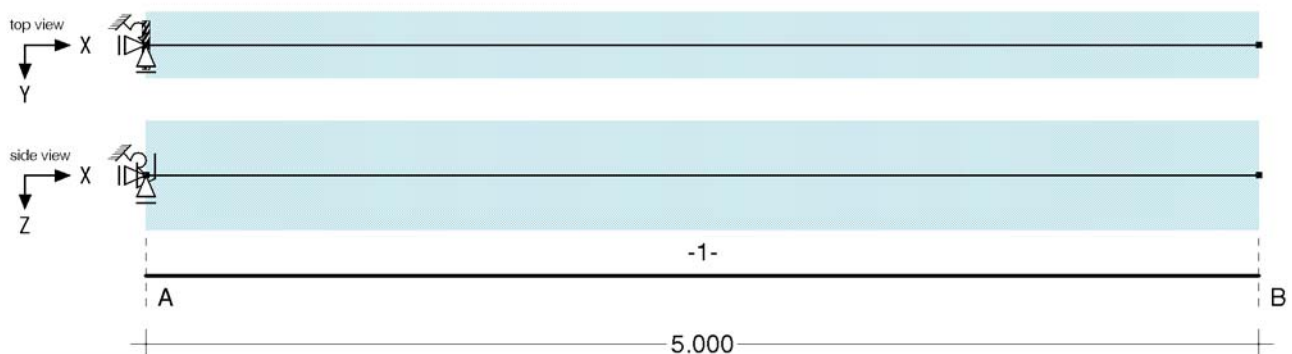
DIN EN 1993-1-1 verification parameters

NA Germany

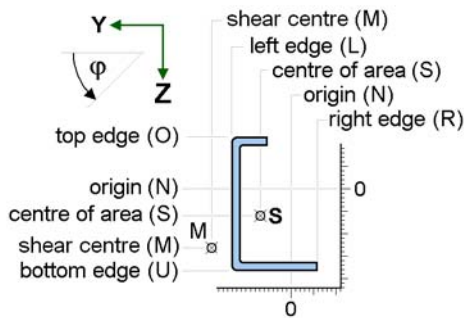
chapter	value	definition
6.1(1)	permanent/transient sit.	partial factors for structural steel
	$\gamma_{M0} = 1.00$	collapse of cross-sections
	$\gamma_{M1} = 1.10$	instability
	accidental situation	partial factors for structural steel
	$\gamma_{M0} = 1.00$	collapse of cross-sections
	$\gamma_{M1} = 1.00$	instability

System sketch

with point bearings of the section ends and position of the point/lines/hinged springs within the sections



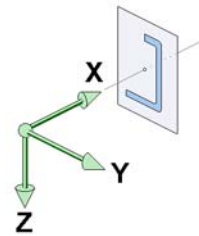
List of sections



The penetration point of the global X-axis through the plane of the cross-section is defined using the alongside shown horizontal and vertical alignment points.

The alignment points are also used to describe the points of action of flexible point or line supports.

Following the alignment the cross-section is rotated through φ about the global X-axis.



sec.	from xa	to xe	l	Orientation at the beginning		Orientation at the end		φ
-	m	m	m	horizontal	vertical	horizontal	vertical	°
1	0.00	5.00	5.00	(S) + 0.00 cm	(S) + 0.00 cm	(S) + 0.00 cm	(S) + 0.00 cm	0.00

Bars with normed steel sections

section	material	γ _{M,E}	st. section name
-	-	-	-
1	S355	1.10	HE500A

section properties of bar sections

The position of the centre of gravity eY , eZ and the angle of rotation α of the principal axes η , ζ or the distance YSM , ZSM of the shear centre from the centroid of gravity is described with respect to the global XYZ system. All other cross-section values are given in the principal axis system

sec.	eY	eZ	α	YSM	ZSM	A	I _η	I _ζ	I _T	I _ω	iM	r _η	r _ζ	r _ω
-	cm	cm	°	cm	cm	cm ²	cm ⁴	cm ⁴	cm ⁴	cm ⁶	cm	cm	cm	-
1	0.00	0.00	0.00	-0.00	0.00	198.00	86970	10370	310.00	5643000	22.17	-0.00	0.00	-0.00

Point supports at the ends of sections

The support is relocated from the X-axis with ΔY and ΔZ and distorted with the angle φ . Numeric values indicate spring constants. CPX, CPY and CPZ describe the bearings for the forces in the indexed direction. CMX, CMY and CMZ describe the moment restraint around the indexed axes. CMΩ is the warping restraint.

support at x	CPX	CPY	CPZ	CMX	CMY	CMZ	CMΩ	ΔY	ΔZ	φ
-	kN/m	kN/m	kN/m	kNm/-	kNm/-	kNm/-	kN/m ³	cm	cm	°
A 0.00	fix	fix	fix	fix	fix	fix	fix	0.00	0.00	0.00

Description of loading structure

On the left-hand side, the relationship between the actions effects, load case file and load cases are shown in a tree structure. The right-hand side shows the characteristics of the superposition to the associated objects on the left-hand. In terms of the superposition, a load case file is equivalent to an extreme rule of the defined objects therein and can be additive or alternatively superpositioned.

applied symbols: action effect load case file load case imperfection cases

1: permanent loads

1: dead load (1)

imperfection cases

1: imperfection (1)

permanent loads

additive

GRAPHIC OF LOADS OF ACTION EFFECTS

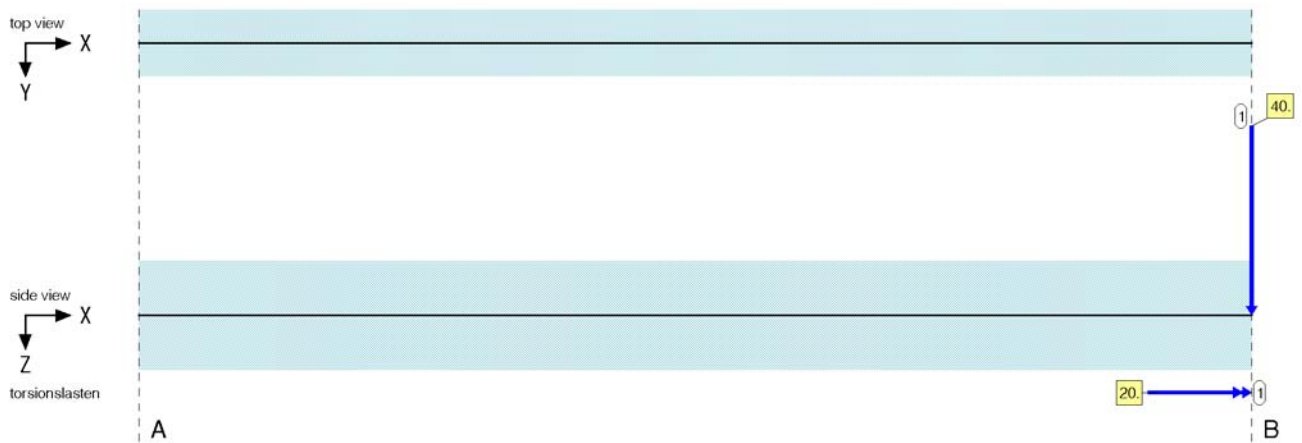
The load images are displayed as projections with regard to the top view (X-Y plane) and the side view (X-Z plane).

Dead loads and torsion loads are drawn separately from the views in a separate line.

The load case numbers are indicated on the individual load images.

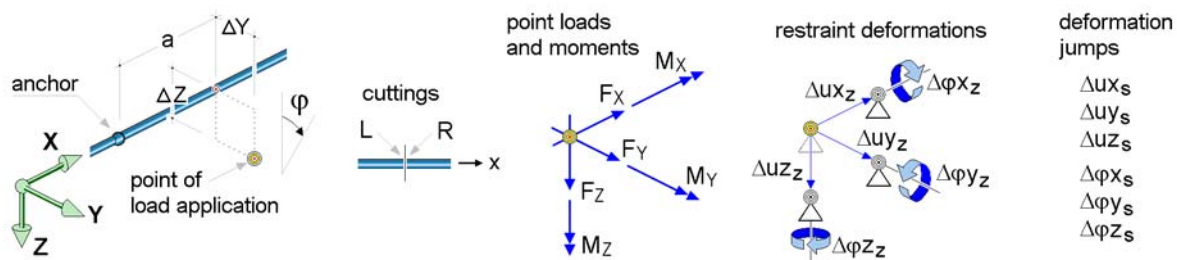
action effect 1: permanent loads

permanent, 1 load case (see numbers of load cases)



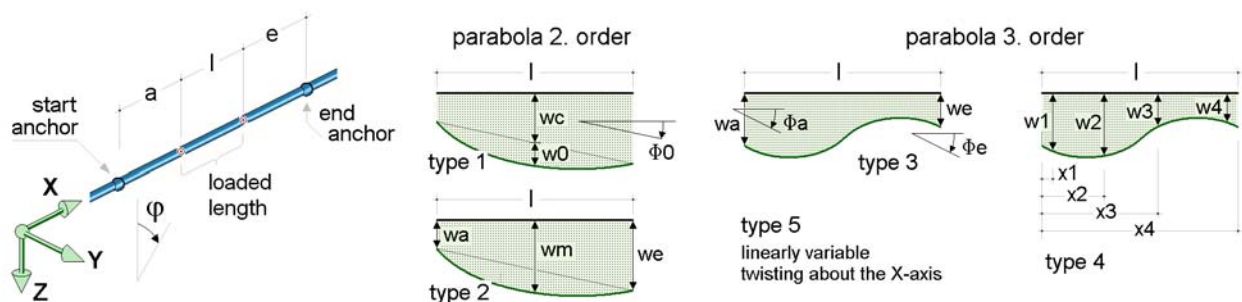
DESCRIPTION OF THE LOAD PICTURES

List of point loads



load case	anchor	a m	ΔY cm	ΔZ cm	bank	load type, ordinates				φ °
1	B	0.000	0.000	0.000	L	F _Z =	40.000 kN	M _Y =	0.000 kNm	0.00
1	B	0.000	0.000	0.000	L	F _X =	0.000 kN	M _X =	20.000 kNm	0.00

Explanation of the types of description for imperfections



Imperfections: type of description 2

imperf. case	start anchor	a m	line sections l m	e m	end anchor	direction	φ °	wa mm	wm mm	we mm
1	A	0.000	5.000	0.000	B	Y	0.00	0.000	1/-500	0.000
1	A	0.000	5.000	0.000	B	Y	0.00	0.000	1/400	1/200

Meanings in the case of application of rules of superposition acc. to Eurocode:

Ψ_{dom}	combination coefficient of a leading traffic load action	(dominant action)
Ψ_{sub}	combination coefficient of a non-leading traffic load action	(accompanying action)
γ_{sup}	Partial safety factor for unfavourable load positions	
γ_{inf}	Partial safety factor for favourable load positions	

rules of superposition bridge construction and DIN 1055-100 behave like Eurocode.
In non-linear analysis, rules of extremization will not be considered

If verifications according to Eurocode are listed below, the following applies:
The national annex "Germany" is taken into account.

verification 1: EC3 design resistance (th. II. o.)

EC 3 design resistance (th. II. o.): design resistance acc. to DIN EN 1993

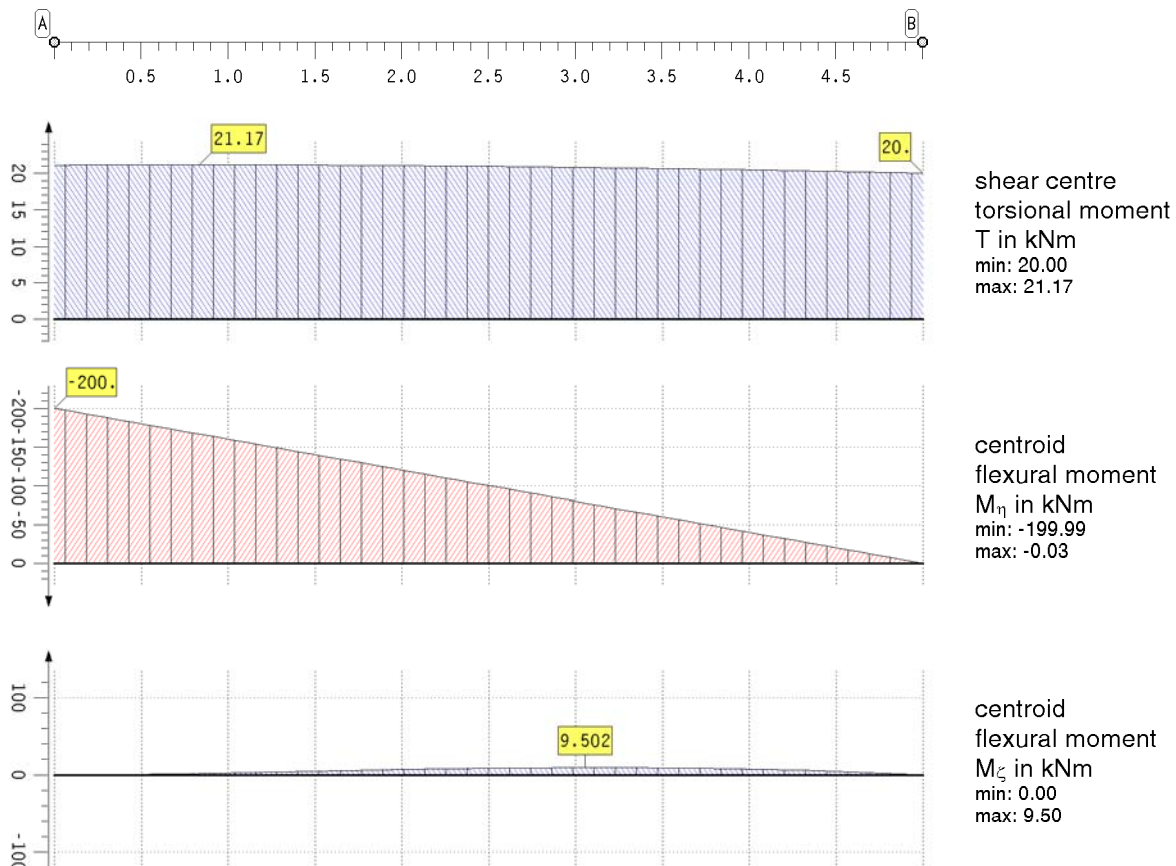
load spectra for verification 1

Factorization of load cases. Negative numbers of load cases refer to imperfections

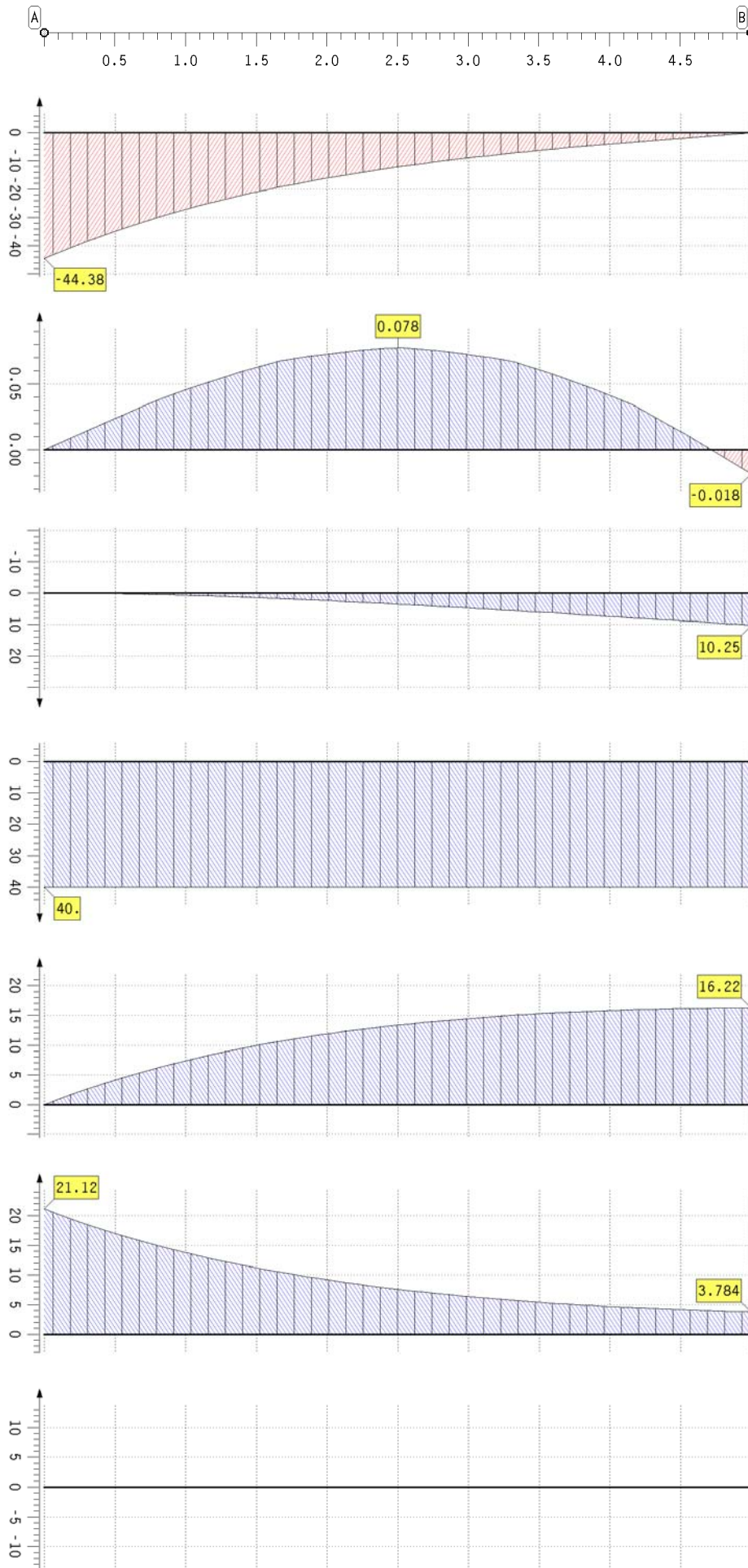
LS	1	-1
1	1.00	1.00

SUMMARY VERIFICATION 1: EC3 DESIGN RESISTANCE (TH. II. O.)

extremal internal forces and moments in system of principal axis



extremal internal forces and moments in system of principal axis



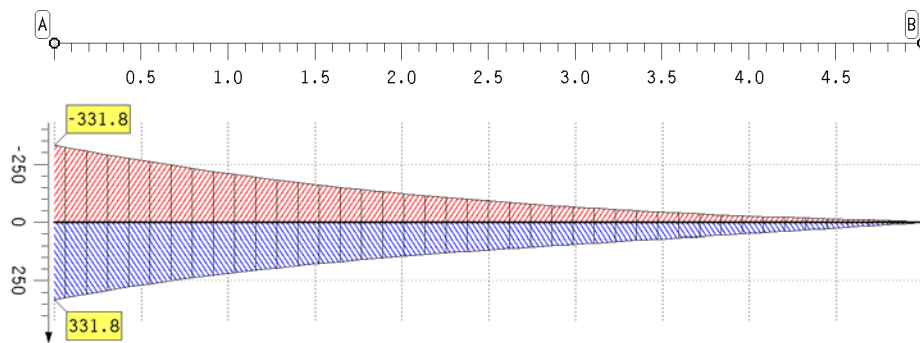
extremal internal forces and moments in system of principal axis

Shear forces V_η , V_ζ , torsional moments T , T_t , T_w , T_σ and warping bimoment B act in the shear centre.

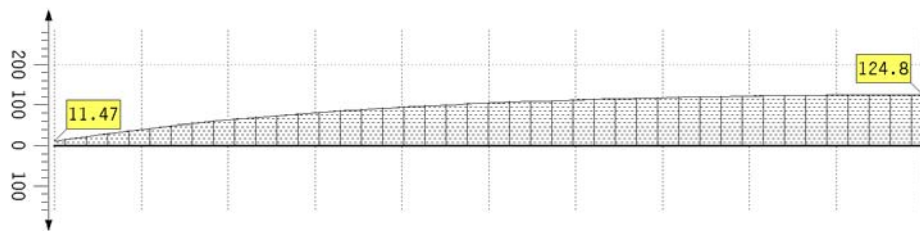
Normal force N and flexural moments M_η , M_ζ refer to the centroid.

point	x	type	N	V_η	V_ζ	T	M_η	M_ζ	T_t	T_w	T_σ	K_σ	B
-	m		kN	kN	kN	kNm	kNm	kNm	kNm	kNm	kNm	kNm ²	kNm ²
A	0.000	min	0.0	0.00	40.00	21.12	-200.0	0.0	0.00	21.12	0.00	0.00	-44.377
		max	0.0	0.00	40.00	21.12	-200.0	0.0	0.00	21.12	0.00	0.00	-44.377
	0.741	min	0.0	0.40	40.00	21.17	-170.4	1.7	5.85	15.32	0.00	0.00	-30.799
		max	0.0	0.40	40.00	21.17	-170.4	1.7	5.85	15.32	0.00	0.00	-30.799
	1.667	min	0.1	1.77	40.00	21.11	-133.3	5.9	10.66	10.45	0.00	0.00	-19.115
		max	0.1	1.77	40.00	21.11	-133.3	5.9	10.66	10.45	0.00	0.00	-19.115
	2.500	min	0.1	3.54	40.00	20.95	-100.0	8.8	13.38	7.58	-0.00	-0.00	-12.045
		max	0.1	3.54	40.00	20.95	-100.0	8.8	13.38	7.58	-0.00	-0.00	-12.045
	3.056	min	0.1	4.91	40.00	20.80	-77.8	9.5	14.59	6.22	-0.00	-0.00	-8.567
		max	0.1	4.91	40.00	20.80	-77.8	9.5	14.59	6.22	-0.00	-0.00	-8.567
B	3.241	min	0.1	5.38	40.00	20.74	-70.4	9.4	14.90	5.84	-0.00	-0.00	-7.528
		max	0.1	5.38	40.00	20.74	-70.4	9.4	14.90	5.84	-0.00	-0.00	-7.528
	4.167	min	0.0	7.90	40.00	20.39	-33.4	6.6	15.93	4.46	0.00	0.00	-3.231
		max	0.0	7.90	40.00	20.39	-33.4	6.6	15.93	4.46	0.00	0.00	-3.231
	5.000	min	-0.0	10.25	40.00	20.00	-0.0	0.0	16.22	3.78	0.00	0.00	-0.000
		max	-0.0	10.25	40.00	20.00	-0.0	0.0	16.22	3.78	0.00	0.00	-0.000
	minimum		-0.0	0.00	40.00	20.00	-200.0	0.0	0.00	3.78	-0.00	-0.00	-44.377
	maximum		0.1	10.25	40.00	21.17	-0.0	9.5	16.22	21.12	0.00	0.00	-0.000

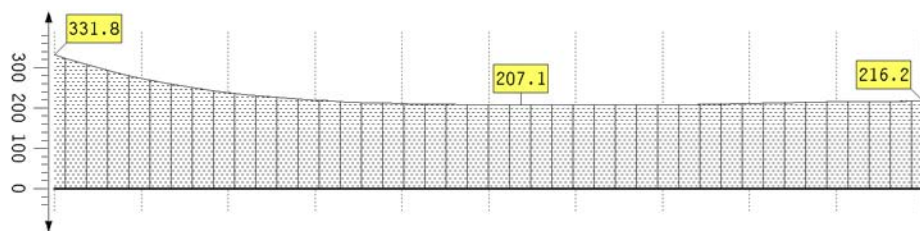
Results of steel design



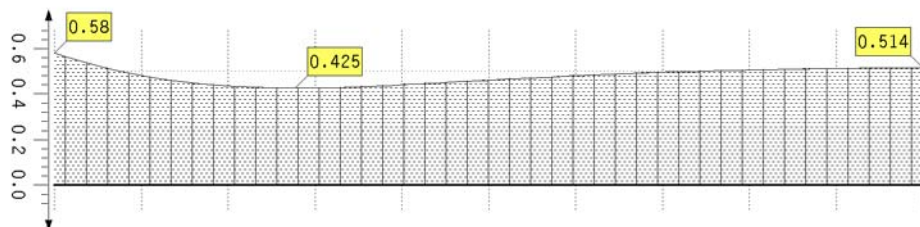
elastic
edge stresses
 σ_x in MN/m²
min: -331.78
max: 331.78



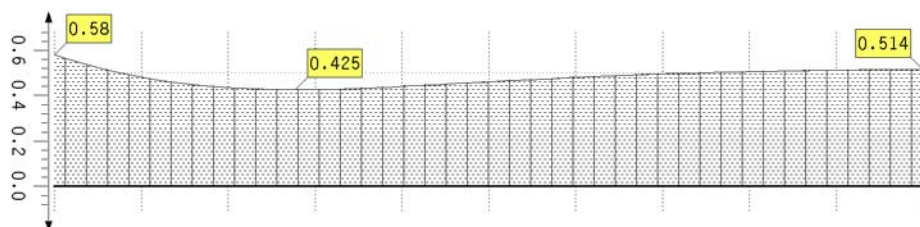
elastic
shear stress
 τ in MN/m²
max: 124.83



elastic
equivalent tensile stress
 σ_v in MN/m²
max: 331.78



plastic
utilization $U_{\sigma,pl}$
of cross-section
max: 0.58



utilization
max: 0.58

Results of steel design

stresses are calculated elastically.

point	x	min σ_x	max σ_x	τ	σ_y	σ_{el}	$U_{\sigma,el}$	$U_{\sigma,p1}$	0-0	--0	U
-	m	MN/m ²	MN/m ²	MN/m ²	MN/m ²	MN/m ²	-	-	-	-	-
A	0.000	-331.78	331.78	11.47	331.78	----	----	0.580	----	----	0.580
	0.648	-247.49	251.38	47.89	260.21	----	----	0.460	----	----	0.460
	1.389	-171.72	185.02	77.33	221.31	----	----	0.425	----	----	0.425
	2.593	-84.99	111.07	106.41	207.15	----	----	0.465	----	----	0.465
B	5.000	-0.02	0.02	124.83	216.21	----	----	0.514	----	----	0.514
minimum		-331.78	0.02	11.47	207.15	0.00	0.000	0.425	0.000	0.000	0.425
maximum		-0.02	331.78	124.83	331.78	0.00	0.000	0.580	0.000	0.000	0.580

Reactions in support points bzgl. der beam axis (γ_F -fach)

point	X	type	AP _x	AP _y	AP _z	AM _x	AM _y	AM _z	AB _x
-	m		kN	kN	kN	kNm	kNm	kNm	kNm ²
A	0.000	min	0.00	-0.00	-40.00	-21.12	199.99	-0.00	44.38
		max	0.00	-0.00	-40.00	-21.12	199.99	-0.00	44.38
B	5.000	min	0.00	0.00	0.00	0.00	0.00	-0.00	-0.00
		max	0.00	0.00	0.00	0.00	0.00	-0.00	-0.00

SUMMARY

Utilizations

