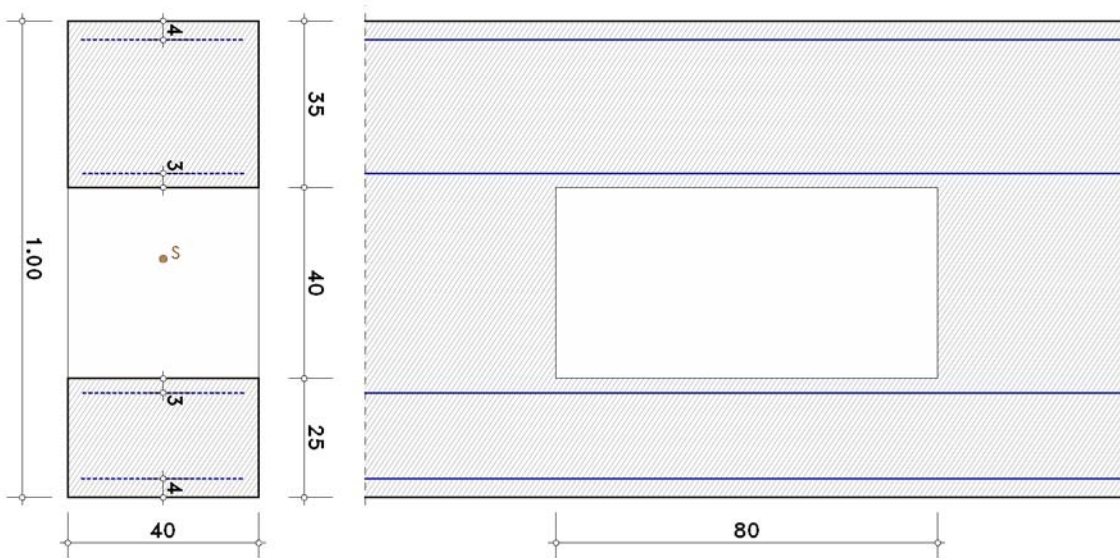


1. input protocol



cross section

rectangle: $h = 100.0$ cm, $b = 40.0$ cm

recess: $e_o = 35.0$ cm, $e_u = 25.0$ cm, $l_A = 80.0$ cm

axis distances (calculation): $d_{o,o} = 4.0$ cm, $d_{u,o} = 3.0$ cm, $d_{o,u} = 3.0$ cm, $d_{u,u} = 4.0$ cm

material properties

concrete acc. to EC 2, 3.1.7(1): C30/37, $\epsilon_{c2} = -2.00\%$, $\epsilon_{cu2} = -3.50\%$, $f_{cd} = 17.00$ N/mm²

reinforcement acc. to EC 2, 3.2.7(2a): B500A, $\epsilon_{ud} = 25.0\%$, $f_{yd} = 434.78$ N/mm², $f_{td} = 456.52$ N/mm², $E_s = 200000.0$ N/mm²

parameters

base reinforcement: top chord above $A_{s0,o} = 0.00$ cm², bottom chord bottom $A_{su,o} = 6.00$ cm²

design method acc. to Heft 459, DAfStb

shear force distribution determined from the gross belt stiffnesses

shear design: compression strut angle minimum

1.1. design calculation values

lc 1: $M_{y,Ed} = 168.00$ kNm, $V_{z,Ed} = -330.00$ kN

2. note

general reinforcement rules are not taken into account.

3. recess

3.1. lc 1

design calculation values in centre cut: $N_{Ed} = 0.00$ kN, $M_{Ed} = 168.00$ kNm, $V_{Ed} = -330.00$ kN

shear force distribution: 73.3% of shear force acts in the compression chord (= top chord)

above the recess

design calculation values in top chord: $N_{Ed,o} = -240.0$ kN, $V_{Ed,o} = -241.9$ kN, $M_{Ed,ol} = 104.6$ kNm, $M_{Ed,or} = -88.9$ kNm

longitudinal reinforcement in top chord: $A_{s0,o} = 4.48$ cm², $A_{su,o} = 5.73$ cm²

shear design:

design resistance without shear reinforcement $V_{Rdc} = 83.07$ kN, max. design resistance of compression strut $V_{Rd,mx} = 579.18$ kN

$V_{Rdc} < |V_{Ed,o}| < V_{Rd,mx} \Rightarrow$ shear reinforcement in top chord: $a_{sb,o} = 10.48$ cm²/m

below the recess

design calculation values in bottom chord: $N_{Ed,u} = 240.0$ kN, $V_{Ed,u} = -88.1$ kN, $M_{Ed,ul} = 38.1$ kNm, $M_{Ed,ur} = -32.4$ kNm

longitudinal reinforcement in bottom chord: $A_{s0,u} = 6.23$ cm², $A_{su,u} = 7.17$ cm²

shear design:

design resistance without shear reinforcement $V_{Rdc} = 23.94$ kN, max. design resistance of compression strut $V_{Rd,mx} = 275.40$ kN

$V_{Rdc} < |V_{Ed,u}| < V_{Rd,mx} \Rightarrow$ shear reinforcement in bottom chord $a_{sb,u} = 3.75$ cm²/m

suspended reinforcement: $A_{s,l} = A_{s,r} = A_{s1} + A_{s2} = 15.43$ cm²

anchoring the chord reinforcement: $T_{v1} = 241.9$ kN $\Rightarrow A_{s1} = 5.56$ cm², distribution width 32.5 cm

transmission of the anchoring forces: $T_{v2} = 429.0$ kN $\Rightarrow A_{s2} = 9.87$ cm², distribution width 90.0 cm

total: $A_{s0,o} = 4.48$ cm², $A_{su,o} = 5.73$ cm², $a_{sb,o} = 10.48$ cm²/m, $A_{s0,u} = 6.23$ cm², $A_{su,u} = 7.17$ cm²

$a_{sb,u} = 3.75$ cm²/m, $A_{s1} = 5.56$ cm², $A_{s2} = 9.87$ cm², $A_{s,l} = A_{s,r} = 15.43$ cm², $\rho = 0.59\%$

4. final result

maximum reinforcement: $A_{so,o} = 4.48 \text{ cm}^2$, $A_{su,o} = 5.73 \text{ cm}^2$, $a_{sb,o} = 10.48 \text{ cm}^2/\text{m}$, $A_{so,u} = 6.23 \text{ cm}^2$
 $A_{su,u} = 7.17 \text{ cm}^2$, $a_{sb,u} = 3.75 \text{ cm}^2/\text{m}$, $A_{s1} = 5.56 \text{ cm}^2$, $A_{s2} = 9.87 \text{ cm}^2$, $A_{s,l} = A_{s,r} = 15.43 \text{ cm}^2$
 $\rho = 0.59\%$

incl. base reinforcement: $A_{so,o} = 4.48 \text{ cm}^2$, $A_{su,o} = 7.17 \text{ cm}^2$

design resistance ensured

5. regulations

EN 1990, Eurocode 0: Grundlagen der Tragwerksplanung;

Deutsche Fassung EN 1990:2002 + A1:2005 + A1:2005/AC:2010, Ausgabe Dezember 2010

EN 1990/NA, Nationaler Anhang zur EN 1990, Ausgabe Dezember 2010

EN 1992-1-1, Eurocode 2: Bemessung und Konstruktion von Stahlbeton- und Spannbetonbauteilen -

Teil 1-1: Allgemeine Bemessungsregeln und Regeln für den Hochbau;

Deutsche Fassung EN 1992-1-1:2004 + AC:2010, Ausgabe Januar 2011

EN 1992-1-1/NA, Nationaler Anhang zur EN 1992-1-1, Ausgabe April 2013

Hermann U. Hottmann, Kurt Schäfer: Bemessen von Stahlbetonbalken und -wandscheiben mit Öffnungen,

Deutscher Ausschuss für Stahlbeton, Heft 459, Beuth Verlag GmbH, 1996