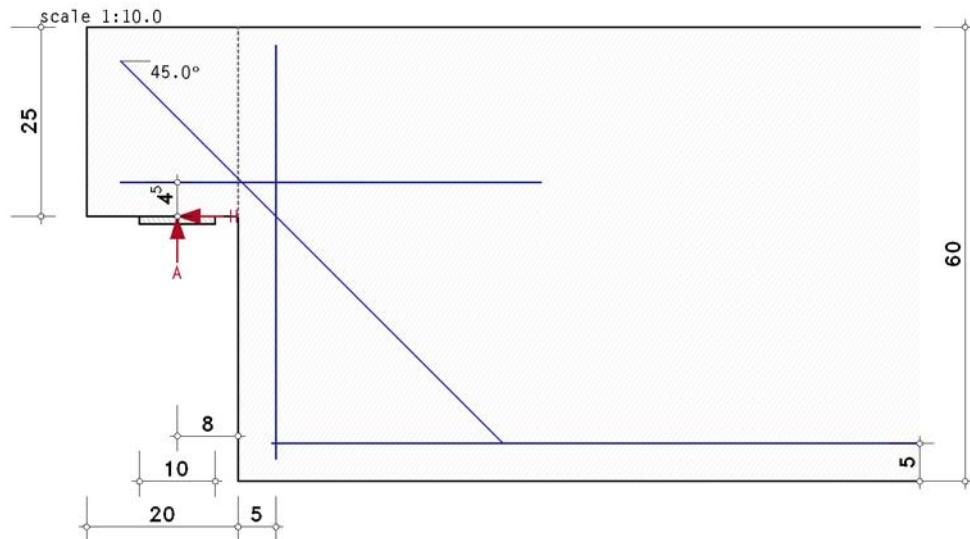


# POS. 24: BEARING BRACKET M. TRANSVERSE REINFORCEMENT

dimensioning a bearing bracket EC 2 (1.11), NA: Deutschland

## 1. input protocol



### cross section (single bracket)

beams:  $b = 23.0 \text{ cm}$ ,  $h = 60.0 \text{ cm}$ , center distance (design calculation):  $d_1 = 5.0 \text{ cm}$   
bracket:  $l_k = 20.0 \text{ cm}$ ,  $h_k = 25.0 \text{ cm}$ , center distance (design calculation):  $d_{1k} = 4.5 \text{ cm}$   
bearing plate:  $l_p = 10.0 \text{ cm}$ ,  $b_p = 20.0 \text{ cm}$

### material properties

concrete: C40/50, reinforcement: B500A

### material safety factors

design situation: basic combination

design resistance: concrete  $\gamma_c = 1.50$ , reinforcement  $\gamma_s = 1.15$

### parameters

Load application for  $\Delta a = 8.0 \text{ cm}$ ,  $\Delta h = 0.0 \text{ cm}$

design method acc. to F. Leonhardt

bearing bracket, load application with variant 2

allocation number 0.58 (load percentage of vertical reinforcement)

inclination angle of transverse reinforcement  $45.0^\circ$

bearing contact pressure: bearing joint of a plain/elastomeric bearing

### design calculation values (ULS)

Ic 1:  $A_{Ed} = 125.0 \text{ kN}$ ,  $H_{Ed} = 25.0 \text{ kN}$

## 2. note

general reinforcement rules are not taken into account.

## 3. design calculation

### 3.1. Ic 1

#### method no longer state of the art !

design calculation values:  $A = A_v = 125.00 \text{ kN}$  ( $\Delta a = 8.0 \text{ cm}$ ),  $H = A_h = 25.00 \text{ kN}$  ( $\Delta h = 0.0 \text{ cm}$ )

bearing contact pressure (plain/elastomeric bearing):  $\sigma_p = 6.25 \text{ N/mm}^2 < \sigma_{Rd,max} = 18.13 \text{ N/mm}^2$  **ok**

load percentage of vertical reinforcement  $A_v = 0.58 \cdot A = 72.50 \text{ kN}$

tensile reinforcement horizontal:  $Z_{A+H} = 114.30 \text{ kN} \Rightarrow \text{req } A_{s,h} = 2.63 \text{ cm}^2$

vertical:  $Z_v = 60.90 \text{ kN} \Rightarrow \text{req } A_{s,v} = 1.40 \text{ cm}^2$

dimensions of beam nose:

58% vertical suspension: min  $h_k = 5.6 \text{ cm} < h_k$  **ok**

42% transverse suspension: min  $d_k = 4.0 \text{ cm} < d_k$  **ok**

verification of compression strut: min  $b = 7.8 \text{ cm} < b$  **ok**

tensile splitting reinforcement:  $A_{sb,h}$  and  $A_{sb,v}$  constructive

load percentage of transverse reinforcement  $A_s = 52.50 \text{ kN}$  at  $\alpha = 45.0^\circ$

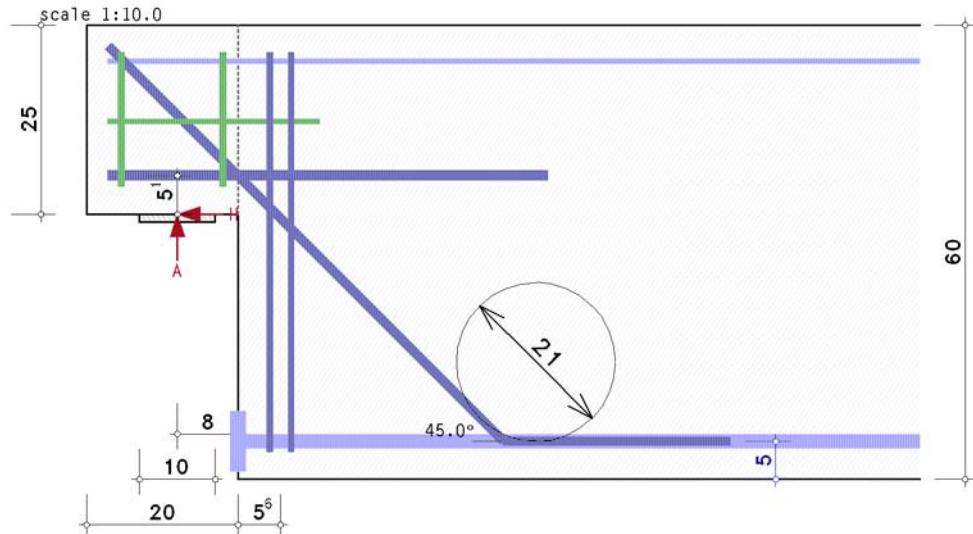
tensile reinforcement transverse:  $Z_s = 74.25 \text{ kN} \Rightarrow \text{req } A_{s,s} = 1.71 \text{ cm}^2$

total:  $A_{s,h} = 2.63 \text{ cm}^2$ ,  $A_{s,v} = 1.40 \text{ cm}^2$ ,  $A_{s,s} = 1.71 \text{ cm}^2$  ( $\Sigma A_{st} = 5.74 \text{ cm}^2$ )

## 4. final result

maximum reinforcement:  $A_{s,h} = 2.63 \text{ cm}^2$ ,  $A_{s,v} = 1.40 \text{ cm}^2$ ,  $A_{s,s} = 1.71 \text{ cm}^2$

## 5. selected reinforcement



calculation of the required anchorage lengths: bonding conditions good

concrete cover  $c_{v,v} = 3.6 \text{ cm}$

concrete cover  $c_{v,h} = 2.8 \text{ cm}$

bottom reinforcement above rod reinforcement, 2Ø8, exst  $A_{so} = 1.01 \text{ cm}^2$

bottom reinforcement bottom rod reinforcement, 3Ø20, exst  $A_{su} = 9.42 \text{ cm}^2$

anchorage length: req  $l_v = 20.0 \text{ cm} > \text{exst } l_v = 4.6 \text{ cm}$  **not ok !!**

main reinforcement 1Ø14,  $D_{min} = 5.6 \text{ cm}$ , exst  $A_{s,h} = 3.08 \text{ cm}^2 > \text{req } A_{s,h} = 2.63 \text{ cm}^2$  **ok**

(U-bents, 2-shear) anchorage lengths: bracket req  $l_v = 16.5 \text{ cm} > \text{exst } l_v = 14.2 \text{ cm}$  **not ok !!**

beams  $l_v = 35.3 \text{ cm}$

transverse reinforcement 1Ø12,  $D_{min,hor} = 4.8 \text{ cm}$ ,  $D_{min,ver} = 21.0 \text{ cm}$ , exst  $A_{s,s} = 2.26 \text{ cm}^2 > \text{req } A_{s,s} = 1.71 \text{ cm}^2$  **ok**

(U-bents, 2-shear) anchorage lengths: bracket req  $l_v = 18.7 \text{ cm} < \text{exst } l_v = 20.1 \text{ cm}$  **ok**

beams  $l_v = 30.0 \text{ cm}$

tensile splitting reinforcement horizontal 1Ø8 (U-bents, 2-shear), exst  $A_{sb,h} = 1.01 \text{ cm}^2$

anchorage length:  $l_v = 8.0 \text{ cm} \Rightarrow$  length of U-bents:  $l_s = 29.0 \text{ cm}$

tensile splitting reinforcement vertical 2Ø8 (stirrup, 2-shear), exst  $A_{sb,v} = 2.01 \text{ cm}^2$

vertical reinforcement 2Ø8 (stirrup, 2-shear), exst  $A_{s,v} = 2.01 \text{ cm}^2 > \text{req } A_{s,v} = 1.40 \text{ cm}^2$  **ok**

anchoring horiz. 2Ø10 (U-bents, 2-shear), exst  $A_{s,h1} = 3.14 \text{ cm}^2$

anchoring vertical 2Ø8 (stirrup, 2-shear), exst  $A_{s,v1} = 2.01 \text{ cm}^2$

center distance exst  $d_{1k} = 5.10 \text{ cm} > \text{clc } d_{1k} = 4.5 \text{ cm}$  **!!**

center distance exst  $e_1 = 5.60 \text{ cm} > \text{clc } e_1 = 5.0 \text{ cm}$  **!!**

center distance exst  $d_{1s} = 5.00 \text{ cm}$  (anchoring of transverse reinforcement in the beam)

check center distance, calculation model does not correspond to the design !

**design resistance not guaranteed !!**

s. selected reinforcement

## 6. regulations

EN 1990, Eurocode 0: Grundlagen der Tragwerksplanung;

Deutsche Fassung EN 1990:2002 + A1:2005 + A1:2005/AC:2010, Ausgabe Dezember 2010

EN 1990/NA, Nationaler Anhang zur EN 1990, Ausgabe Dezember 2010

EN 1992-1-1, Eurocode 2: Bemessung und Konstruktion von Stahlbeton- und Spannbetonbauteilen -

Teil 1-1: Allgemeine Bemessungsregeln und Regeln für den Hochbau;

Deutsche Fassung EN 1992-1-1:2004 + AC:2010, Ausgabe Januar 2011

EN 1992-1-1/NA, Nationaler Anhang zur EN 1992-1-1, Ausgabe April 2013

Fritz Leonhardt, Eduard Mönnig: Vorlesungen über Massivbau, Zweiter Teil,  
Sonderfälle der Bemessung im Stahlbetonbau, Dritte Auflage, Springer-Verlag, 1986

Fritz Leonhardt, Eduard Mönnig: Vorlesungen über Massivbau, Dritter Teil,  
Grundlagen zum Bewehren im Stahlbetonbau, Dritte Auflage, Springer-Verlag, 1977