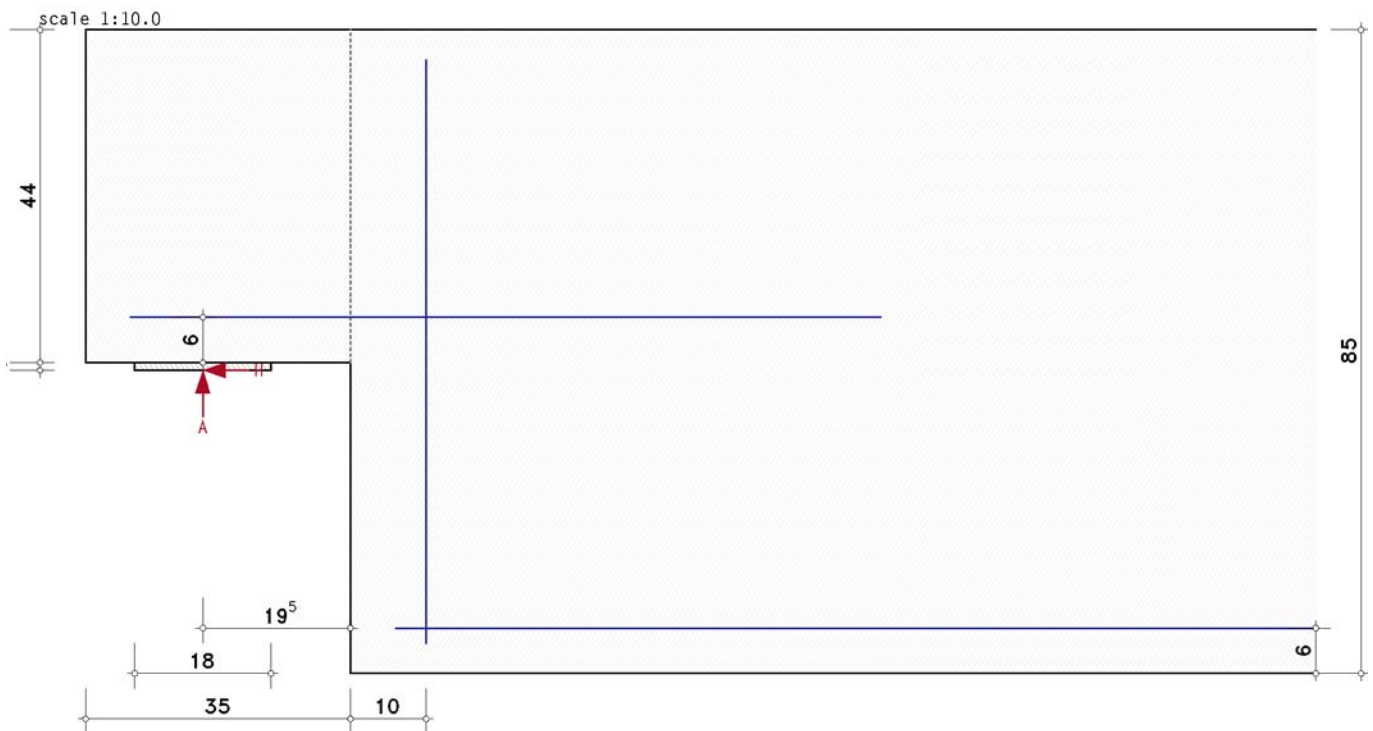


1. input protocol



cross section (single bracket)

beams: $b = 35.0$ cm, $h = 85.0$ cm, center distance (design calculation): $d_1 = 6.0$ cm

bracket: $l_k = 35.0$ cm, $h_k = 44.0$ cm, center distance (design calculation): $d_{1k} = 6.0$ cm

bearing plate: $l_p = 18.0$ cm, $b_p = 20.0$ cm

material properties

concrete acc. to EC 2, 3.1.7(1): C35/45, $\varepsilon_{c2} = -2.00\text{‰}$, $\varepsilon_{cu2} = -3.50\text{‰}$, $f_{cd} = 19.83$ N/mm²

reinforcement acc. to EC 2, 3.2.7(2a): B500A, $\varepsilon_{ud} = 25.0\text{‰}$, $f_{yd} = 434.78$ N/mm², $f_{td} = 456.52$ N/mm², $E_s = 200000.0$ N/mm²

material safety factors

design situation: basic combination

design resistance: concrete $\gamma_c = 1.50$, reinforcement $\gamma_s = 1.15$

parameters

Load application for $\Delta a = 19.5$ cm, $\Delta h = 1.0$ cm

design method acc. to issue 600, DAfStb

bearing bracket, load application with variant 1

bearing contact pressure: bearing joint of a plain/elastomeric bearing

design calculation values (ULS)

Ic 1: $A_{Ed} = 200.0$ kN, $H_{Ed} = 40.0$ kN

2. note

general reinforcement rules are not taken into account.

3. design calculation

3.1. Ic 1

variant 1

beam cross-section

width $b = 35.0$ cm, height $h = 85.0$ cm

bracket cross-section

height $h_k = 44.0$ cm

bearing plate

length $l_p = 18.0$ cm, width $b_p = 20.0$ cm

axis distances

$d_1 = 6.0$ cm, $d_{1k} = 6.0$ cm ($z_k = 33.9$ cm, $z_Q = 34.2$ cm)

$e_1 = 10.0$ cm $\Rightarrow e = \Delta a + e_1 = 29.5$ cm

design calculation acc. to issue 600, DAfStb

design calculation values: $A = A_v = 200.00$ kN ($\Delta a = 19.5$ cm), $H = A_h = 40.00$ kN ($\Delta h = 1.0$ cm)

bearing contact pressure (plain/elastomeric bearing): $\sigma_p = 5.56$ N/mm² $< \sigma_{Rd,max} = 16.86$ N/mm² **ok**

verification of compression strut: $V_{Ed} = 200.0$ kN $< V_{Rd,max} = 733.2$ kN **ok**

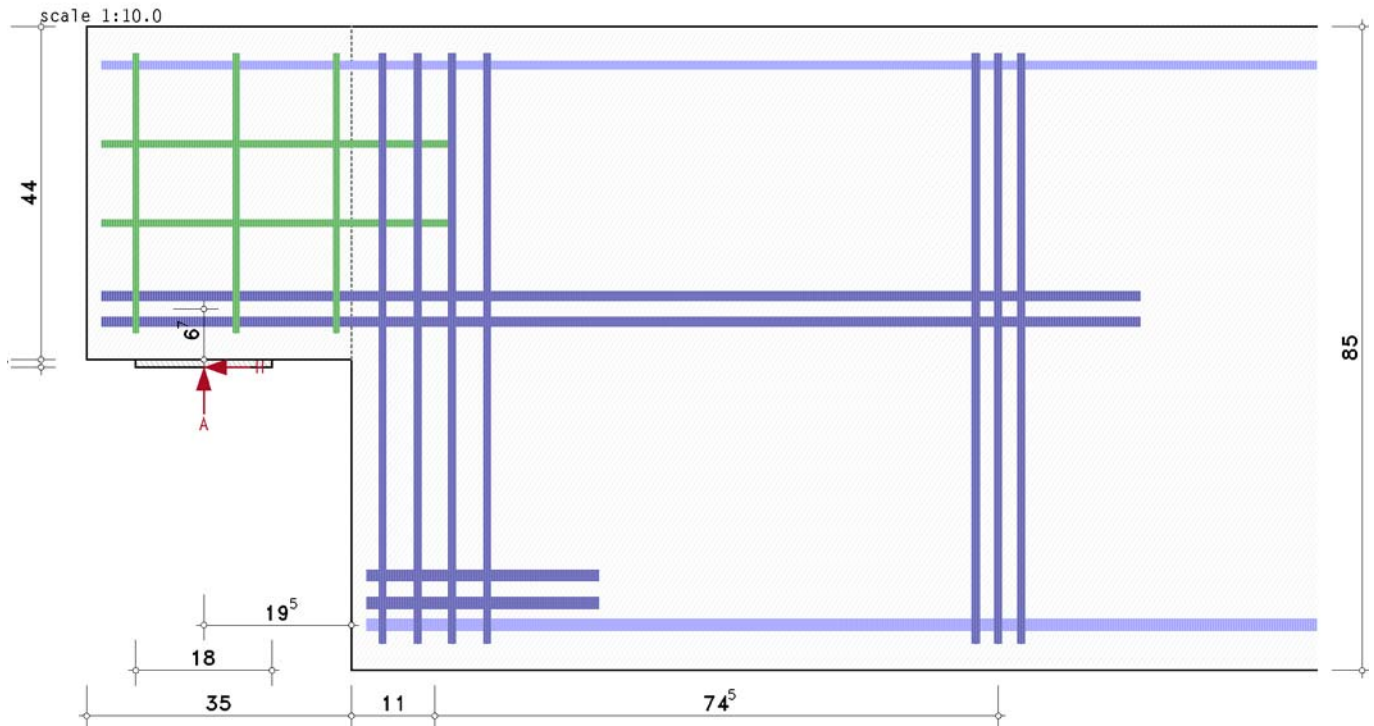
tensile reinforcement horizontal: $Z_{A+H} = 222.55$ kN $\Rightarrow \text{req } A_{s,h} = 5.12$ cm²

vertical: $Z_V = 200.00 \text{ kN} \Rightarrow \text{req } A_{s,v} = 4.60 \text{ cm}^2$
 anchoring of $A_{s,h}$: $Z_{V,1} = 107.35 \text{ kN} \Rightarrow \text{req } A_{s,v1} = 2.47 \text{ cm}^2$ at $z_3 = 74.5 \text{ cm}$
 tensile splitting reinforcement: $A_{sb,h}$ and $A_{sb,v}$ constructive for $\Delta a/d_k > 0.5$ and $V_{Ed} < V_{Rd,c} = 219.95 \text{ kN}$
 anchoring of bottom reinforcement req $A_{s,h1} = \text{req } A_{s,h} = 5.12 \text{ cm}^2$
 total: $A_{s,h} = 5.12 \text{ cm}^2$, $A_{s,v} = 4.60 \text{ cm}^2$, $A_{s,h1} = 5.12 \text{ cm}^2$, $A_{s,v1} = 2.47 \text{ cm}^2$ at $z_3 = 74.5 \text{ cm}$
 ($\Sigma A_{st} = 9.72 \text{ cm}^2$)

4. final result

maximum reinforcement: $A_{s,h} = 5.12 \text{ cm}^2$, $A_{s,v} = 4.60 \text{ cm}^2$, $A_{s,h1} = 5.12 \text{ cm}^2$, $A_{s,v1} = 2.47 \text{ cm}^2$ at $z_3 = 74.5 \text{ cm}$

5. selected reinforcement



calculation of the required anchorage lengths: calculate bonding conditions

concrete cover to vertical stirrup reinforcement $c_{v,v} = 3.5 \text{ cm}$

concrete cover to main reinforcement $c_{v,h} = 2.0 \text{ cm}$

bottom reinforcement above rod reinforcement, $2\text{Ø}12$, exst $A_{so} = 2.26 \text{ cm}^2$

bottom reinforcement bottom rod reinforcement, $6\text{Ø}16$, exst $A_{su} = 12.06 \text{ cm}^2$

anchorage length: req $l_v = 21.9 \text{ cm} > \text{exst } l_v = 16.4 \text{ cm} \Rightarrow \text{anchoring } A_{s,h1} \text{ req. !!}$

main reinforcement 1. Lage: $1\text{Ø}14$, $D_{\min} = 5.6 \text{ cm}$, exst $A_{s,h} = 3.08 \text{ cm}^2$

(U-bents, 2-shear) 2. Lage: $1\text{Ø}14$, $D_{\min} = 5.6 \text{ cm}$, exst $A_{s,h} = 3.08 \text{ cm}^2$, $d_v = 3.4 \text{ cm}$

exst $A_{s,h} = 6.16 \text{ cm}^2 > \text{req } A_{s,h} = 5.12 \text{ cm}^2$ ok

anchorage lengths: bracket req $l_v = 17.5 \text{ cm} < \text{exst } l_v = 22.5 \text{ cm}$ ok

beams $l_v = 37.5 \text{ cm}$

length of U-bents: $l_s = 145.5 \text{ cm}$

tensile splitting reinforcement horizontal $2\text{Ø}10$ (U-bents, 2-shear), exst $A_{sb,h} = 3.14 \text{ cm}^2$

anchorage length: $l_v = 10.0 \text{ cm} \Rightarrow \text{length of U-bents: } l_s = 46.6 \text{ cm}$

tensile splitting reinforcement vertical $3\text{Ø}8$ (stirrup, 2-shear), exst $A_{sb,v} = 3.02 \text{ cm}^2$

vertical reinforcement $4\text{Ø}10$ (stirrup, 2-shear), exst $A_{s,v} = 6.28 \text{ cm}^2 > \text{req } A_{s,v} = 4.60 \text{ cm}^2$ ok

anchoring horiz. $2\text{Ø}16$ (U-bents, 2-shear), exst $A_{s,h1} = 8.04 \text{ cm}^2 > \text{req } A_{s,h1} = 5.12 \text{ cm}^2$ ok

anchorage length: req $l_v = 16.4 \text{ cm} \leq \text{exst } l_v = 16.4 \text{ cm}$ ok

lap length $l_v = 30.7 \text{ cm}$

anchoring vertical $3\text{Ø}10$ (stirrup, 2-shear), exst $A_{sb,v1} = 4.71 \text{ cm}^2 > \text{req } A_{sb,v1} = 2.47 \text{ cm}^2$ ok

center distance exst $d_{1k} = 6.70 \text{ cm} > \text{clc } d_{1k} = 6.0 \text{ cm}$!! with minimum bar distance each layer

center distance exst $e_1 = 11.00 \text{ cm} > \text{clc } e_1 = 10.0 \text{ cm}$!! with bar distance $d_h = 4.60 \text{ cm} > \text{min } d_h = 3.0 \text{ cm}$ ok

check center distance, calculation model does not correspond to the design !

design resistance ensured

6. regulations

EN 1990, Eurocode 0: Grundlagen der Tragwerksplanung;

Deutsche Fassung EN 1990:2002 + A1:2005 + A1:2005/AC:2010, Ausgabe Dezember 2010

EN 1990/NA, Nationaler Anhang zur EN 1990, Ausgabe Dezember 2010

EN 1992-1-1, Eurocode 2: Bemessung und Konstruktion von Stahlbeton- und Spannbetonbauteilen -

Teil 1-1: Allgemeine Bemessungsregeln und Regeln für den Hochbau;

Deutsche Fassung EN 1992-1-1:2004 + AC:2010, Ausgabe Januar 2011

EN 1992-1-1/NA, Nationaler Anhang zur EN 1992-1-1, Ausgabe April 2013

Erläuterungen zu DIN EN 1992-1-1 and DIN EN 1992-1-1/NA, Teil 1

Deutscher Ausschuss für Stahlbeton, Heft 600, Beuth Verlag GmbH, 2020

Erläuterungen zu DIN 1045-1

Deutscher Ausschuss für Stahlbeton, Heft 525, Beuth Verlag GmbH, 2003