

POSITION 5: STIEL/Z/STB-DBL.

1. Input parameters

1.1. Fasteners

dowel 16 mm, S235 (1052)

$F_{v,Rd}$ calculated with the simplified verification acc. to NA.8.2.4

connection rafter/collar beam: 4 x dowel

1.2. Internal forces combination collar beam

Nr	N _d kN	V _d kN	k _{mod} -	A
1	50.00	0.00	0.80	

* in column A in case of accidental combination

2. System visualisation

2.1. Static values and constructive boundary conditions

service class 2, connection angle $\alpha = 90.0^\circ$

rafter of solid coniferous timber, C30 (S13) with $\rho_k = 380 \text{ kg/m}^3$

pair of collar beams of solid coniferous timber, C24 (S10) with $\rho_k = 350 \text{ kg/m}^3$

pair of collar beams : $t = 8.0 \text{ cm}$, $h = 16.0 \text{ cm}$, $A_n = 102.40 \text{ cm}^2$, $W_n = 340.65 \text{ cm}^3$, $I_n = 2725.21 \text{ cm}^4$

rafter: $t = 12.0 \text{ cm}$, $h = 26.0 \text{ cm}$, $A_n = 264.00 \text{ cm}^2$, $W_n = 1215.67 \text{ cm}^3$, $I_n = 15317.44 \text{ cm}^4$

connection collar beam/rafter

max $\alpha = 0.0^\circ \Rightarrow$ minimum spacings at collar beam

$a_1 = 8.0 \text{ cm}$, $a_2 = 4.8 \text{ cm}$, $a_{1,t} = 11.2 \text{ cm}$, $a_{1,c} = 0.0 \text{ cm}$, $a_{2,t} = 4.8 \text{ cm}$, $a_{2,c} = 4.8 \text{ cm}$

max $\alpha = 90.0^\circ \Rightarrow$ minimum spacings at rafter

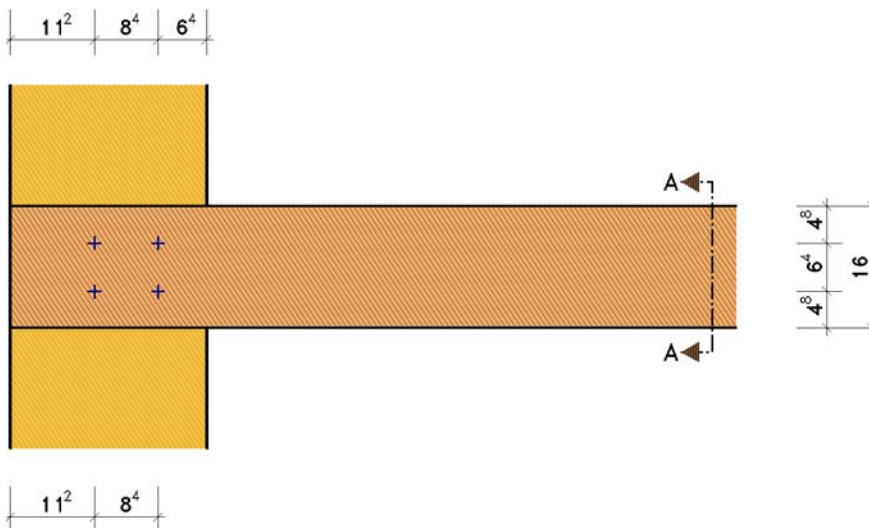
$a_1 = 4.8 \text{ cm}$, $a_2 = 4.8 \text{ cm}$, $a_{1,t} = 11.2 \text{ cm}$, $a_{1,c} = 11.2 \text{ cm}$, $a_{2,t} = 6.4 \text{ cm}$, $a_{2,c} = 4.8 \text{ cm}$

$a_{1,exist} = 8.40 \text{ cm}$, $a_{2,exist} = 6.40 \text{ cm}$

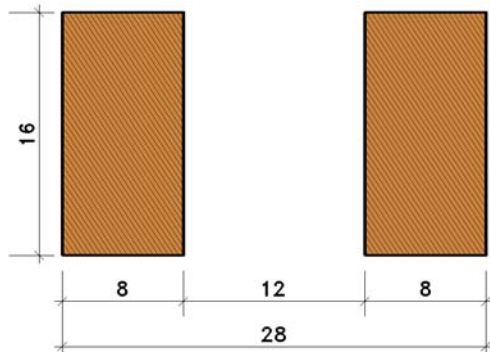
centroid of fasteners from hinge point S at $x_s = 2.40 \text{ cm}$, $y_s = 0.00 \text{ cm}$

polar moment of inertia $I_{p1} = 111.52 \text{ cm}^4$

elevation scale 1:10



section A-A collar beam scale 1: 5



3. Verification of fasteners acc. to DIN EN 1995, NA Germany

$\gamma_{M,outer\ timber\ member} = 1.30$, $\gamma_{M,central\ timber\ member} = 1.30$, $\gamma_{steel} = 1.10$, $\gamma_{accidental} = 1.00$

3.1. Decisive load combination collar beam

3.1.1. Fasteners rafter/collar beam

$N_d = 50.00\text{ kN}$, $V_d = 0.00\text{ kN}$, $M_{v,d} = |0.02 \times 0.00| = 0.00\text{ kNm}$, $k_{mod} = 0.80$

$F_{H1,d} = 50.00 / (2 \times 4) = 6.25\text{ kN}$

$\alpha_{min} = 90.00$, $a_1 = 84\text{ mm}$, $n = 2 \Rightarrow n_{ef} = 1.49$

forces per shear plane ($f_{red} = t_{exist} / t_{req}$)

Nr	F _{H1} kN	F _{MH1} kN	F _{MV1} kN	F _{totH1} kN	F _{totV1} kN	F _{tot1} kN	$\alpha_{tot1,k}$ °	$\alpha_{tot1,s}$ °	f _{h,α,k} N/mm ²	f _{red} -	F _{v,Rk} kN	F _{v,Rd} kN	U -
1	0.00	0.00	0.00	6.25	0.00	6.25	0.00	90.00	16.46	1.000	9.5582	5.1704	1.21

maximum utilization of fasteners $U_{max} = 1.21 > 1 \Rightarrow$ verification not successful

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4. Verification pair of collar beams

4.1. Decisive load combination collar beam

strengths and design resistances for $k_{mod} = 0.80$

pair of collar beams: $f_{t,d} = 5.74\text{ N/mm}^2$, $f_{m,d} = 14.77\text{ N/mm}^2$, $f_{c,d} = 12.92\text{ N/mm}^2$, $f_{v,d} = 1.23\text{ N/mm}^2$

rafter: $f_{t,d} = 11.08\text{ N/mm}^2$, $f_{m,d} = 18.46\text{ N/mm}^2$, $f_{c,d} = 14.15\text{ N/mm}^2$, $f_{v,d} = 1.23\text{ N/mm}^2$

$\sigma_{t,d} = 2.44\text{ N/mm}^2$, $\tau_d = 0.00\text{ N/mm}^2 \Rightarrow U = 0.43$

maximum utilization of pair of collar beams $U_{max} = 0.43 \leq 1 \Rightarrow$ verification successful

5. Summary

maximum utilization of all verifications $U_{max} = 1.21 > 1 \Rightarrow$ verification not successful

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