

# POSITION 8: RAUTENSTRAUCH S. 264

## 1. Input parameters

### 1.1. ribs (vertical), flanges (horizontal)

service class 1

panel width/height = 250.0 / 255.0 cm, sheet edges transmitting shear on all sides

ribs 5.0 / 12.0 cm from solid coniferous timber, C24 (S10) with  $\rho_k = 350 \text{ kg/m}^3$ ,  $a_r = 62.5 \text{ cm}$

flanges 5.0 / 12.0 cm from solid coniferous timber, C24 (S10) with  $\rho_k = 350 \text{ kg/m}^3$

### 1.2. sheathing on one side

OSB 4 with  $\rho_k = 550 \text{ kg/m}^3$ , service class 1,  $t = 18.0 \text{ mm}$

special nail 1A, 2.5 x 50.0 mm,  $d_k = 5.0 \text{ mm}$ ,  $l_{ef} = 50.0 \text{ mm}$ , not predrilled

simplified verification acc. to NA.8.2.4, distance  $a_v = 90 \text{ mm}$ , 1-row

vertical loads transmitted only by ribs

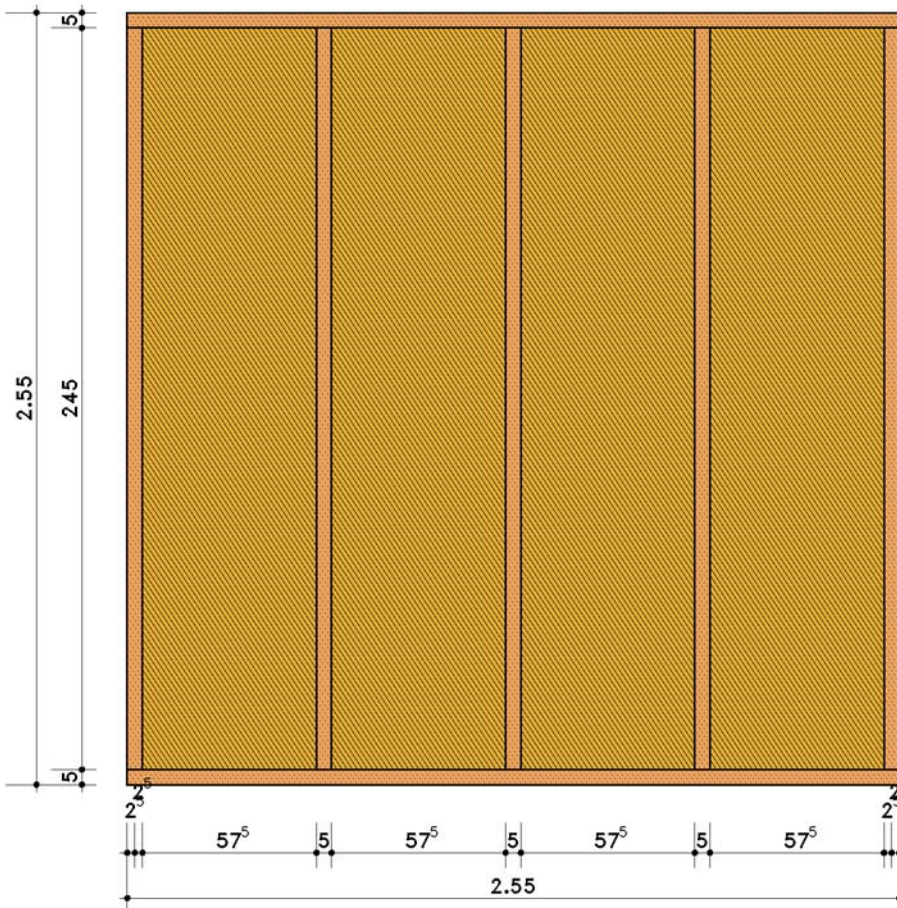
### 1.3. Combinations of internal forces for verifications at ultimate limit state

Nr	$F_{v,d}$ kN	$E_{d1}$ kN/m	$E_{dr}$ kN/m	$F_{1c,d}$ kN	$F_{2c,d}$ kN	$k_{mod,r}$ -	$k_{mod,b1}$ -	A
1	9.180	0.000	2.000	7.950	0.000	0.900	0.900	

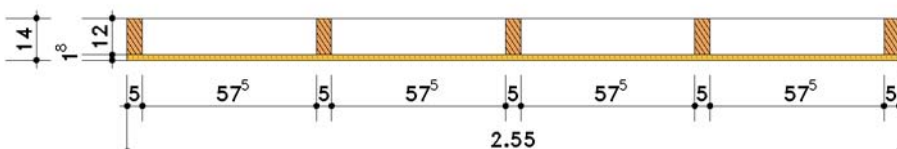
### 1.4. Combinations of internal forces for verifications at serviceability limit state

Nr	$F_{v,k}$ kN	$E_{k1}$ kN/m	$E_{kr}$ kN/m	$F_{1c,k}$ kN	$F_{2c,k}$ kN
1	5.000	0.000	0.000	1.000	1.000

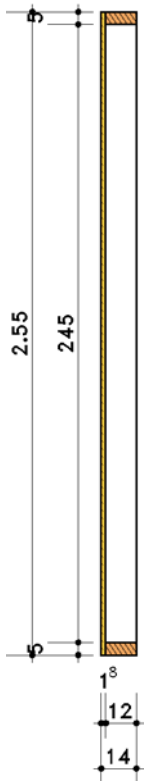
elevation scale 1:25



longitudinal section scale 1:25



transversal section scale 1:30



## 2. verifications acc. to DIN EN 1995, Germany

### 2.1. Fasteners sheathing 1

fastener ends in rib, penetration depth  $t = 32$  mm

$F_{V,Rk}$  increased acc. to DIN EN 1995, 9.2.4.2 (5) (sheet edges transmitting shear on all sides)

$f_{uk} = 450$  N/mm<sup>2</sup>,  $M_{yk} = 1462$  Nmm,  $f_{hk} = 45.70$  N/mm<sup>2</sup>,  $\beta = 0.00$

$F_{V,Rk} = 462.4$  N,  $F_{V,Rd} = 378.3$  N per shear plane,  $\gamma_M = 1.10$

### 2.2. Verification of diaphragm loading

web

$\gamma = 1.30$ ,  $f_{vk} = 6.9$  N/mm<sup>2</sup>,  $f_{ck} = 14.0$  N/mm<sup>2</sup>,  $k_{v1} = 1.00$ ,  $k_{v2} = 0.33$

#### 2.2.1. Load combination 1

wall panel in horizontal diaphragm loading

sheathing 1

$F_{V,Rd} = 378$  N,  $f_{vd} = 4.78$  N/mm<sup>2</sup>,  $f_{cd} = 9.69$  N/mm<sup>2</sup>

$f_{v0d} = 4.20$  N/mm (fastener),  $f_{v90d} = 4.20$  N/mm (fastener)

⇒ utilization:  $U_{0d} = 0.87$ ,  $U_{90} = -1.00$  ⇒  **$U = 0.87$  verification successful**

### 2.3. Verification of compression of bottom edge beam

$A_{ef\ li} = 9600$  mm<sup>2</sup>,  $A_{ef\ inside} = 13200$  mm<sup>2</sup>,  $A_{ef\ re} = 9600$  mm<sup>2</sup>,  $x_1 = 1.00$  DIN 1052, 8.7.5,  $k_{c90} = 1.25$

#### 2.3.1. Load combination 1

$f_{v90d} = 4.20$  N/mm<sup>2</sup>,  $f_{c90d} = 2.08$  N/mm<sup>2</sup>,  $f_{rib} = 1.00$

$\Sigma F_{c,d\ edge} = 17781$  N,  $\Sigma F_{c,d\ inside} = 1105$  N,  $\sigma_{c,d\ li} = 1.85$  N/mm<sup>2</sup>,  $\sigma_{c,d\ inside} = 0.08$  N/mm<sup>2</sup>,  $\sigma_{c,d\ re} = 1.85$  N/mm<sup>2</sup>

⇒ utilization:  **$U = 0.71$  verification successful**

### 2.4. Verification of compression flange

$E_{0,05} = 7333$  N/mm<sup>2</sup>,  $f_{c0k} = 21.0$  N/mm<sup>2</sup>,  $l = 2500$  cm,  $i_r = 14.4$  mm,  $A = 6000$  mm<sup>2</sup>

flanges secured against buckling perpendicular to the wall surface

#### 2.4.1. Load combination 1

$f_{c0d} = 14.54$  N/mm<sup>2</sup>,  $F_{c,d} = 9180$  N,  $\sigma_{c0,d} = 1.53$  N/mm<sup>2</sup>

⇒ utilization:  **$U = 0.11$  verification successful**

### 2.5. verification of vertical Borderribs

$f_{c0k} = 21.0$  N/mm<sup>2</sup>,  $h = 255$  cm,  $i_r = 34.7$  mm,  $A = 6000$  mm<sup>2</sup>

$k = 1.380$ ,  $k_c = 0.511$ ,  $\beta_c = 0.200$ ,  $\lambda_{rel,c} = 1.2525$ ,  $\lambda = 73.53$

### 2.5.1. Load combination 1

$f_{c0d} = 14.54 \text{ N/mm}^2$ ,  $\Sigma F_{c,d} = 17781 \text{ N} \Rightarrow \sigma_c = 2.96 \text{ N/mm}^2$   
 $\Rightarrow$  utilization:  $U = 0.40$  verification successful

### 2.6. Verification of vertical ribs (inside)

$f_{c0k} = 21.0 \text{ N/mm}^2$ ,  $h = 255 \text{ cm}$ ,  $i_r = 34.7 \text{ mm}$ ,  $A = 6000 \text{ mm}^2$   
 $k = 1.380$ ,  $k_c = 0.511$ ,  $\beta_c = 0.200$ ,  $\lambda_{rel,c} = 1.2525$ ,  $\lambda = 73.53$

### 2.6.1. Load combination 1

$f_{c0d} = 14.54 \text{ N/mm}^2$ ,  $\Sigma F_{c,d} = 1105 \text{ N} \Rightarrow \sigma_c = 0.18 \text{ N/mm}^2$   
 $\Rightarrow$  utilization:  $U = 0.02$  verification successful

### 2.7. Verification of deformation at ultimate limit state

$k_{ser} = 429.8 \text{ N/mm}$ ,  $k_{c90} = 1.25$ ,  $A_r = 5014.1 \text{ mm}^2$ ,  $l_1 = 575 \text{ mm}$ ,  $u_{zul} = 25.5 \text{ mm}$   
 $G_{mean} = 838.5 \text{ N/mm}^2$ ,  $E_{0,mean} = 8461.5 \text{ N/mm}^2$ ,  $f_{c90} = 1.92 \text{ N/mm}^2$

### 2.7.1. Load combination 1

$\sigma_{c90} = 1.85 \text{ N/mm}^2$ ,  $u_k = 3.11 \text{ mm}$ ,  $u_G = 0.62 \text{ mm}$ ,  $u_E = 0.74 \text{ mm}$ ,  $u_V = 1.31 \text{ mm}$ ,  $K_d = 1588.29 \text{ N/mm}$   
 $\Sigma u = 5.78 \text{ mm} \Rightarrow$  utilization:  $U = 0.23$  verification successful

### 2.8. Verification of deformation at serviceability limit state

$k_{ser} = 838.2 \text{ N/mm}$ ,  $k_{c90} = 1.25$ ,  $A_r = 5014.1 \text{ mm}^2$ ,  $l_1 = 575 \text{ mm}$ ,  $u_{zul} = 17.0 \text{ mm}$   
 $G_{mean} = 1090.0 \text{ N/mm}^2$ ,  $E_{0,mean} = 11000.0 \text{ N/mm}^2$ ,  $f_{c90} = 2.50 \text{ N/mm}^2$

### 2.8.1. Load combination 1

$\sigma_{c90} = 0.53 \text{ N/mm}^2$ ,  $u_k = 0.87 \text{ mm}$ ,  $u_G = 0.26 \text{ mm}$ ,  $u_E = 0.31 \text{ mm}$ ,  $u_V = 0.29 \text{ mm}$ ,  $K_d = 2893.55 \text{ N/mm}$   
 $\Sigma u = 1.73 \text{ mm} \Rightarrow$  utilization:  $U = 0.10$  verification successful

## 3. Summary

maximum utilization of all verifications  $U_{max} = 0.87 \leq 1 \Rightarrow$  all verifications successful