

## 1. Input parameters

### 1.1. girder opening circular with glued-in steel bars acc. to DIN EN 1995-1-1/NA:2013-08, NCI NA.6.8.4

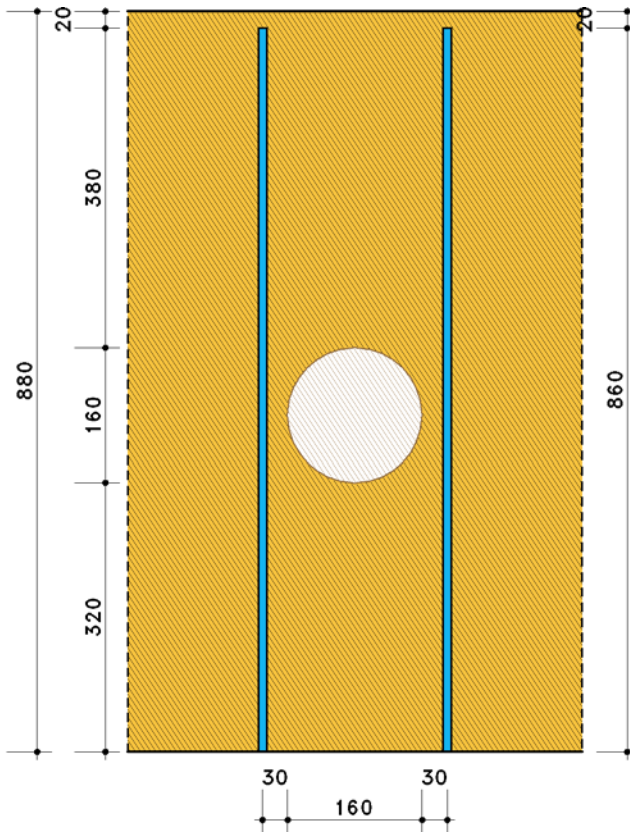
### 1.2. beam

beam of glue laminated timber EC, GL28h 220/880 mm,  $\rho_k = 425 \text{ kg/m}^3$ , NKL 1  
 $h_{ro} = 400 \text{ mm}$ ,  $h_{ru} = 320 \text{ mm}$ ,  $a = 160 \text{ mm}$  (expressions acc. to NA:2013-08, NCI NA.6.7 figure NA.7)  
 $f_{m,k} = 28.00 \text{ N/mm}^2$ ,  $f_{t,k} = 22.30 \text{ N/mm}^2$ ,  $f_{c,k} = 28.00 \text{ N/mm}^2$ ,  $f_{v,k} = 3.50 \text{ N/mm}^2$ ,  $f_{t90,k} = 0.50 \text{ N/mm}^2$   
 $f_{m,k}$  increased with  $k_h = 1.000$

### 1.3. reinforcement by 3 glued in steelbars

$d_r = 10 \text{ mm}$ ,  $d_{ef} = 10.0 \text{ mm}$ ,  $l_e = 860 \text{ mm}$ , BST500A/B,  $a_{3,c} = 30 \text{ mm}$ ,  $a_2 = 30 \text{ mm}$ ,  $a_{4,c} = 30 \text{ mm}$

elevation scale 1:90, unit of length [mm]



### 1.4. internal forces and moments

Nr.	name	left edge			right edge			KLED	k <sub>mod</sub>	γ
		N <sub>d</sub> kN	V <sub>d</sub> kN	M <sub>d</sub> kNm	N <sub>d</sub> kN	V <sub>d</sub> kN	M <sub>d</sub> kNm			
1	g+t+w+s	0.00	409.50	798.53	0.00	392.70	734.35	sh.-term	0.900	1.30

## 2. results

### 2.1. tension stress perpendicular to grain in opening area

$h_r = 344 \text{ mm}$ ,  $l_{t,90} = 496 \text{ mm}$ ,  $f_{t,90k} = 0.500 \text{ N/mm}^2$ ,  $f_{k1,k} = 3.530 \text{ N/mm}^2$ ,  $l_{ad} = 344 \text{ mm}$

Nr	f <sub>t90,d</sub> N/mm <sup>2</sup>	f <sub>k1,d</sub> N/mm <sup>2</sup>	F <sub>t90R,d</sub> kN	N <sub>R,d</sub> kN	left edge				right edge				u
					F <sub>tV,d</sub> kN	F <sub>tM,d</sub> kN	F <sub>t90,d</sub> kN	u <sub>l</sub> -	F <sub>tV,d</sub> kN	F <sub>tM,d</sub> kN	F <sub>t90,d</sub> kN	u <sub>r</sub> kN	
1	0.346	2.444	26.411	31.42	38.88	18.57	57.45	0.725	37.28	17.08	54.36	0.686	0.725

$u_{max} = 0.725 \leq 1 \Rightarrow \text{ok.}$

## 2.2. bending at the opening area cross-section

$I_{nz} = 1234972 \text{ cm}^4$ ,  $z_s = 431 \text{ mm}$ ,  $W_{no} = 28646 \text{ cm}^3$ ,  $W_{nu} = 27512 \text{ cm}^3$ ,  $W_o = 5867 \text{ cm}^3$ ,  $W_u = 3755 \text{ cm}^3$

Nr	$f_{m,d}$ N/mm <sup>2</sup>	$f_{t,d}$ N/mm <sup>2</sup>	$f_{c,d}$ N/mm <sup>2</sup>	$\sigma_{N,d}$ N/mm <sup>2</sup>	$\sigma_{M,o,d}$ N/mm <sup>2</sup>	$\sigma_{M,u,d}$ N/mm <sup>2</sup>	$\sigma_{u,d}$ N/mm <sup>2</sup>	$\sigma_{o,d}$ N/mm <sup>2</sup>	$u_{o,d}$ -	$u_{u,d}$ -	$u$ -
1	19.38	15.44	19.38	0.000	-26.755	27.859	-26.76	27.859	1.380	1.437	1.437

$u_{max} = 1.437 > 1 \Rightarrow$  **not ok. !!**

## 2.3. shear at the reduced cross section in circlemitte

beam width = 220 mm, beam height = 720 mm,  $k_{cr} = 0.714 \Rightarrow A_{ef} = 113143 \text{ mm}^2$ ,  $\kappa_{max} = 1.546$

Nr	$f_{v,d}$ N/mm <sup>2</sup>	$V_d$ kN	$\tau_{m,d}$ N/mm <sup>2</sup>	$u$ -
1	2.42	401.10	5.318	2.195

$u_{max} = 2.195 > 1 \Rightarrow$  **not ok. !!**

## 3. Summary

total utilization all verifications  $u_{max,Ges} = 2.195 > 1 \Rightarrow$  **not ok. !!**