

POSITION 46: BODDENBERG II, T1, BSP 2-1 S.19

1. Input parameters

2. General statements

double shear plane connection, exact verification acc. to DIN EN 1995, 8.2.2
crossing angle $\delta = 180.0^\circ$

3. materials

3.1. outer timber members

NKL 1, glue laminated timber EC GL24h, $\rho_k = 385 \text{ kg/m}^3$, $t/b = 85.0/220.0 \text{ mm}$
angle between force and the grain direction $\alpha = 0.0^\circ$
bar on one side right with overhang $\bar{u}_{\text{right}} = 210.0 \text{ mm}$ (measured from the node)

3.2. centre plate

steel plate S235 (St37), $t = 10.0 \text{ mm}$, steel plate acc. to NA 8.2.5
bar on one side left with overhang $\bar{u}_{\text{right}} = 165.0 \text{ mm}$ (measured from the node)

4. fasteners

dowel 12 mm, S235 (1052)

coordinates of the fasteners (origin in the node, x to the right, y upwards)

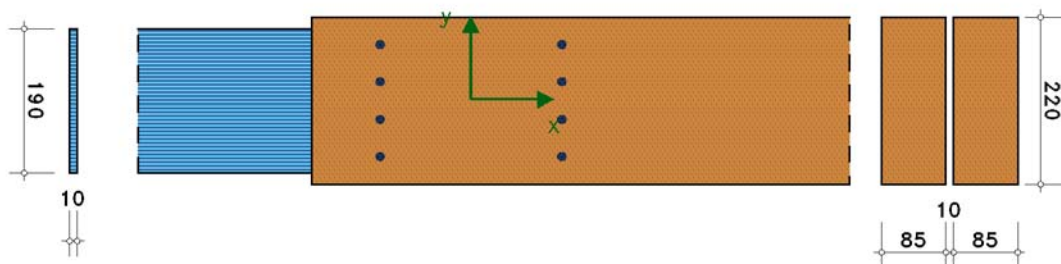
Nr	x _k mm	y _k mm	Nr	x _k mm	y _k mm
1	-120.0	73.5	5	120.0	73.5
2	-120.0	24.5	6	120.0	24.5
3	-120.0	-24.5	7	120.0	-24.5
4	-120.0	-73.5	8	120.0	-73.5

4.1. load combinations (design internal forces)

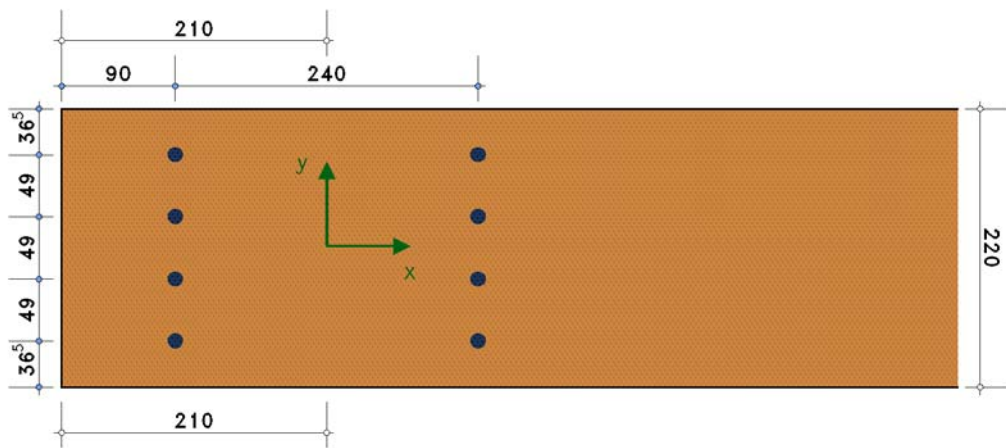
4.1.1. load, KLED: permanent

Nr	bar	N _d kN	M _d kNm	V _d kN	k _{mod} -	γ -
1	out. t. memb. right	0.000	6.800	4.000	0.600	1.30
2	ctr. t.mem. left	0.000	-6.800	4.000	0.000	1.30
3	$\Sigma H, \Sigma M, \Sigma V$	-0.000	0.000	0.000	---	---

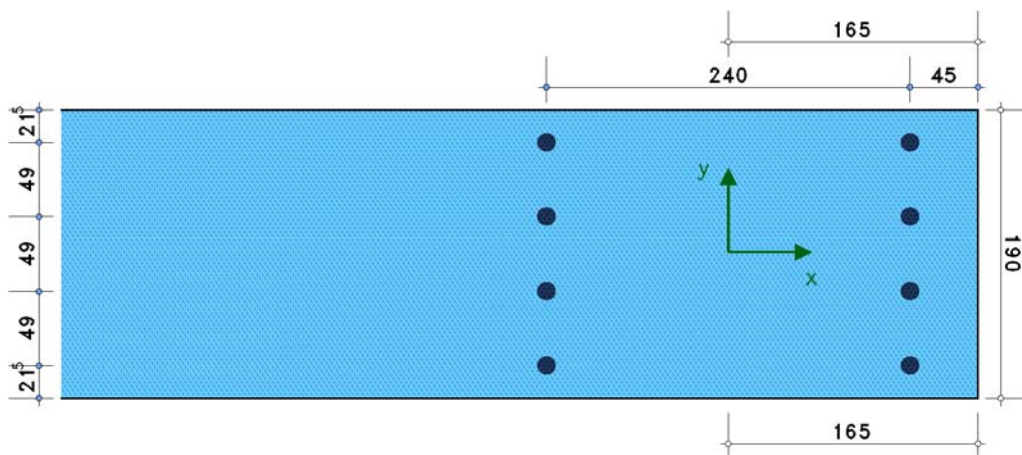
5. view



6. view outer timber members



7. view centre plate



8. Results only decisive load case combination

8.1. Results fasteners

8.2. fasteners

8.2.1. load

$N_d = 0.000$ kN, $V_d = -4.000$ kN, $M_{v,d} = 6.800$ kNm

forces per connection centre point, case = decisive failure case acc. to DIN EN 1995-1-1, 8.2.2

Nr	F_{M1} kN	F_{MH1} kN	F_{MV1} kN	F_{totH1} kN	F_{totV1} kN	F_{tot1} kN	α_{tot1} °	$f_{h,\alpha,k}$ N/mm ²	case	$F_{v,Rd}$ kN	$U_{n,ef}$ -	$U_{F,v}$ -
1	6.874	3.590	-5.862	3.590	-6.362	7.305	-60.6	19.82	G1.(h)	8.6042	0.42	0.85
2	5.983	1.197	-5.862	1.197	-6.362	6.473	-79.3	18.38	G1.(g)	8.2051	0.15	0.79
3	5.983	-1.197	-5.862	-1.197	-6.362	6.473	-100.7	18.38	G1.(g)	8.2051	0.15	0.79
4	6.874	-3.590	-5.862	-3.590	-6.362	7.305	-119.4	19.82	G1.(h)	8.6042	0.42	0.85
5	6.874	3.590	5.862	3.590	5.362	6.453	56.2	20.34	G1.(h)	8.7170	0.41	0.74
6	5.983	1.197	5.862	1.197	5.362	5.494	77.4	18.46	G1.(g)	8.2387	0.15	0.67
7	5.983	-1.197	5.862	-1.197	5.362	5.494	102.6	18.46	G1.(g)	8.2387	0.15	0.67
8	6.874	-3.590	5.862	-3.590	5.362	6.453	123.8	20.34	G1.(h)	8.7170	0.41	0.74

maximum utilisation of the fasteners $U_{max} = 0.85 \leq 1 \Rightarrow$ verification fulfilled

8.3. results bars

8.3.1. outer timber member mit $A_n = 29240$ mm², $W_n = 1147805$ mm³, $I_n = 126258547$ mm⁴, $k_h = 1.100$

load	$f_{m,d}$ N/mm ²	$f_{t,d}$ N/mm ²	$f_{c,d}$ N/mm ²	$f_{v,d}$ N/mm ²	N_d kN	M_d kNm	$\sigma_{0,d}$ N/mm ²	$\sigma_{m0,d}$ N/mm ²	$\sigma_{mu,d}$ N/mm ²	V_d kN	τ_d N/mm ²	U_σ -	U_τ -
1	12.18	9.75	11.08	1.62	0.000	6.800	0.00	5.92	5.92	25.447	2.28	0.49	1.41

maximum utilisation of the bar $U_{max} = 1.41 > 1 \Rightarrow$ verification not fulfilled

!!

8.3.2. central timber member mit $A_n = 1420 \text{ mm}^2$, $W_n = 44942 \text{ mm}^3$, $I_n = 4269473 \text{ mm}^4$, $k_h = 0.000$

load	$f_{y,d}$ N/mm ²	$f_{v,d}$ N/mm ²	N_d kN	M_d kNm	$\sigma_{y,d}$ N/mm ²	V_d kN	$\tau_{v,d}$ N/mm ²	$\sigma_{sv,d}$ N/mm ²	$U_{\sigma sv}$ -	U_{σ} -	U_{τ} -
1	235.00	135.68	0.000	-6.800	-151.31	25.447	26.88	158.31	0.67	0.64	0.20

maximum utilisation of the bar $U_{\max} = 0.67 \leq 1 \Rightarrow$ **verification fulfilled**

8.4. Punched hole forces

$p_1 = 240 \text{ mm}$, $e_1 = 22 \text{ mm}$, $e_2 = 22 \text{ mm}$, $p_2 = 49.00 \text{ mm}$, $\alpha_b = 1.00$, $k_1 = 2.50 \Rightarrow F_{b,Rk} = 108.00 \text{ kN}$
 $e_1 = 22 \text{ mm}$, $e_2 = 22 \text{ mm}$, $p_2 = 49 \text{ mm}$, $\alpha_b = 0.60$, $k_1 = 2.50 \Rightarrow F_{b,Rk,Rand} = 64.50 \text{ kN}$

8.4.1. load

Nr	F_{toti} kN	$F_{v,Rd}$ kN	U -	Nr	F_{toti} kN	$F_{v,Rd}$ kN	U -
1	7.30	51.60	0.14	5	6.45	51.60	0.13
2	6.47	51.60	0.13	6	5.49	86.40	0.06
3	6.47	51.60	0.13	7	5.49	86.40	0.06
4	7.30	51.60	0.14	8	6.45	51.60	0.13

maximum utilisation of the punched hole forces $U_{\max} = 0.14 \leq 1 \Rightarrow$ **verification fulfilled**

8.5. verification of block shear failure acc. to DIN EN 1995-1-1, annex A

$L_{net,t} = 147 \text{ mm}$, $t_1 = 85 \text{ mm} \Rightarrow A_{net,t} = 12495 \text{ mm}^2$, $M_{y,k} = 69070.9 \text{ Nmm}$

$L_{net,v} = 660 \text{ mm}$, $t_{ef} = 85 \text{ mm} \Rightarrow A_{net,v} = 56100 \text{ mm}^2$ (failure mechanism c,f,j/l,k,m)

$L_{net,v} = 660 \text{ mm} \Rightarrow A_{net,v} = 56100 \text{ mm}^2 \Rightarrow F_{bs,Rk} = 395.84 \text{ kN}$

8.5.1. load

load	N_d kN	$F_{bs,Rd}$ kN	U_{bs} -
1	0.000	182.696	0.00

maximum utilisation block shear failure $U_{\max} = 0.00 \leq 1 \Rightarrow$ **verification fulfilled**